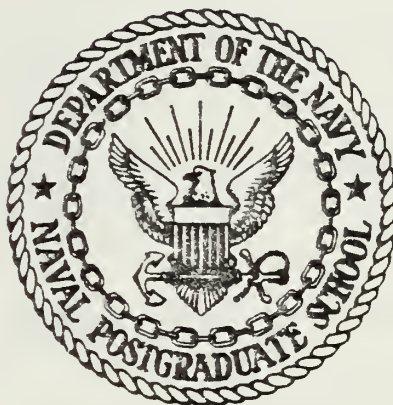


THEORETICAL ANALYSIS OF
TRANSONIC FLOW PAST
UNSTAGGERED OSCILLATING CASCADES

Peter Carlton Olsen

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

THEORETICAL ANALYSIS OF
TRANSONIC FLOW PAST
UNSTAGGERED OSCILLATING CASCADES

by

Peter Carlton Olsen

September 1978

Thesis Advisor:

M.F. Platzer

Approved for public release; distribution unlimited.

T185395

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Theoretical Analysis of Transonic Flow Past Unstaggered Oscillating Cascades		5. TYPE OF REPORT & PERIOD COVERED Engineer's Thesis September 1978
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) Peter Carlton Olsen		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		12. REPORT DATE September 1978
		13. NUMBER OF PAGES 134
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Naval Postgraduate School Monterey, California 93940		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Oscillating Airfoil Transonic Flow Collocation Solution Potential Flow		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This paper presents an independent verification of the collocation method as a technique for calculating the lift on an oscillating airfoil in an unstaggered cascade immersed in transonic flow. This method was		

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE
S/N 0102-014-6601

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

(20. ABSTRACT Continued)

originally proposed by Gorelov. Results presented here differ somewhat from those presented by him. Two formulations are shown; one is purely numerical, the second employs an analytic expansion for small frequency.

UNCLASSIFIED

Approved for public release; distribution unlimited.

Theoretical Analysis of
Transonic Flow Past
Unstaggered Oscillating Cascades

by

Peter Carlton Olsen
Lieutenant, United States Coast Guard
B.S., United States Coast Guard Academy, 1970
M.S., University of West Florida, 1975
M.S.A.E., Naval Postgraduate School, 1977
M.S.O.R., Naval Postgraduate School, 1978

Submitted in partial fulfillment of the
requirements for the degree of

AERONAUTICAL ENGINEER

from the

NAVAL POSTGRADUATE SCHOOL

September 1978

Phew
0484
C.1

ABSTRACT

This paper presents an independent verification of the collocation method as a technique for calculating the lift on an oscillating airfoil in an unstaggered cascade immersed in transonic flow. This method was originally proposed by Gorelov. Results presented here differ somewhat from those presented by him. Two formulations are shown; one is purely numerical, the second employs an analytic expansion for small frequency.

TABLE OF CONTENTS

I.	INTRODUCTION -----	14
II.	UNSTEADY TRANSONIC FLOW THEORY -----	16
III.	SMALL PERTURBATION THEORY OF TRANSONIC FLOW -	23
	A. GENERAL CASE -----	23
	B. BOUNDARY CONDITION -----	25
	C. NONDIMENSIONALIZATION -----	26
	D. HARMONIC OSCILLATIONS -----	29
IV.	LINEARIZATION OF THE GOVERNING EQUATION -----	31
	A. BASIC SOLUTION -----	31
	B. BOUNDARY CONDITIONS -----	34
	C. INITIAL CONDITIONS -----	34
V.	PROBLEM FORMULATION -----	36
	A. CO-ORDINATE SYSTEM -----	36
	B. BOUNDARY CONDITIONS -----	37
	1. Upstream Condition -----	37
	2. Flow Tangency Condition -----	37
	C. BASIC SOLUTION TECHNIQUE -----	38
	D. COLLOCATION SOLUTION OF THE POTENTIAL EQUATION EXPANDED FOR SMALL k -----	51
	1. Solution for the Unknown Potential Coefficients -----	51
	2. Calculation of the Potential -----	57
VI.	RESULTS -----	63
VII.	RECOMMENDATIONS -----	70
	APPENDIX A. PROGRAM DESCRIPTION -----	73

LIST OF REFERENCES -----	133
INITIAL DISTRIBUTION LIST -----	134

LIST OF SYMBOLS

a	= local speed of sound	II
a _o	= speed of sound in the uniform flow	III
c	= blade semichord	III
f _j	= elementary function used in collocation solution	V
F	= specific energy ("head")	II
G	= function describing the surface of the airfoil as a function of time	III
H	= function specifying location of blade surface in the vertical axis	III
i	= $\sqrt{-1}$	II, III, IV, V
k	= Strouhal number, nondimensional frequency	III, IV, V
m	= $\sqrt{(\gamma+1)w}$	IV, V
M	= Mach number = $\frac{ \vec{V} }{a}$	III
n	= number of collocation points - 1, order of highest spanning function	V
p	= pressure	II
	= nondimensional interblade distance	V
R	= universal gas constant	II
R.P.	= "real part of"	III, IV, V
T	= temperature	II
t	= time, nondimensional time	II, III, IV, V
U _o	= uniform velocity from infinity	II, III, VI
u	= x-component of velocity	II, III
u ^o , u ¹	= interference vertical velocities due to reference and adjacent blades respectively, solved so as to satisfy the tangential flow conditions	V, VI

u'	= small disturbance velocity	III
v	= y-component of velocity	II,III,IV,V
\vec{V}	= general velocity vector	II
v'	= small disturbance velocity	III
v^0, v^1	= vertical velocities due to the reference and adjacent blades respectively, determined from the tangential flow condition	V
w	= $\tilde{\phi}_x$, a constant used in Gorelov's approximation of the transonic flow potential	IV,V
x	= horizontal coordinate, may be non-dimensional	
x_*	= mp (transformed interblade distance in Gorelov's approximation)	V
x_l	= blade leading edge	IV
x_0	= center of pitch of the unstaggered cascade	IV,V
y	= vertical coordinate, may be non-dimensional	
y, y_1	= vertical coordinates attached to the reference and adjacent blades respectively, may be non-dimensional	IV,V
z, z_1	= transformed vertical coordinates used in Gorelov's approximation, attached to the reference and adjacent blades respectively. $z = my, z_1 = my_1$	IV,V
$\frac{D}{Dt}$	= substantial derivative w.r.t. time $= \frac{\partial}{\partial t} + \frac{\partial x}{\partial t} \frac{\partial}{\partial x} + \frac{\partial y}{\partial t} \frac{\partial}{\partial y}$ $= \frac{\partial}{\partial t} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y}$	II,III
$O(\omega^2)$	= "of the order of magnitude of ω^2 "	V
α	= angle of attack	II,III,IV,V
α_0	= maximum amplitude of pitch oscillations	IV

γ	= ratio of specific heats, c_p/c_v	
δ_{io}	= Dirac Delta function = 1 when $i = 0$ = 0 when $i \neq 0$	V
η	= $\cos^{-1}(-x)$	V
η_*	= $\cos^{-1}(1-x_*)$	V
$\bar{\eta}$	= $\cos^{-1}(-s)$	V
$\hat{\eta}$	= $\cos^{-1}(x_*-x)$	V
θ_j^0, θ_j^1	= interference potential coefficients for reference and adjacent blades respectively	V
λ	= k/m^2	IV,V
μ_j^0, μ_j^1	= Fourier coefficients describing the motion of the reference and adjacent blades respectively	V
ν	= angular frequency of oscillation	IV,V
ρ	= density	II
σ	= phase angle	V
τ	= cascade solidity, $\frac{2}{p}$	V
Φ	= general velocity potential	II,III,VI
Φ_0	= uniform flow velocity potential	
$\tilde{\Phi}$	= steady flow perturbation potential	III,IV
Φ^0, Φ^1	= perturbation potential in collocation solution due to reference and adjacent blades respectively	V,VI
ϕ^0, ϕ^1	= transformed potentials	V
ψ	= oscillatory flow potential	III,IV,V
ϕ	= transformed oscillatory potential in Gorelov's coordinates corresponding to ψ	V
ψ^0, ψ^1	= interference potentials due to reference and adjacent blades respectively	V,VI

ψ^0, ψ^1 = transformed potentials in Gorelov's coordinates, corresponding to ψ^0 and ψ^1 V

$$\omega = \frac{k(1-m)^2}{m^4}$$

∇ = $\vec{i} \frac{\partial}{\partial x} + \vec{j} \frac{\partial}{\partial y}$, Gradient operator, \vec{i} and \vec{j} are unit vectors in the x and y direction respectively

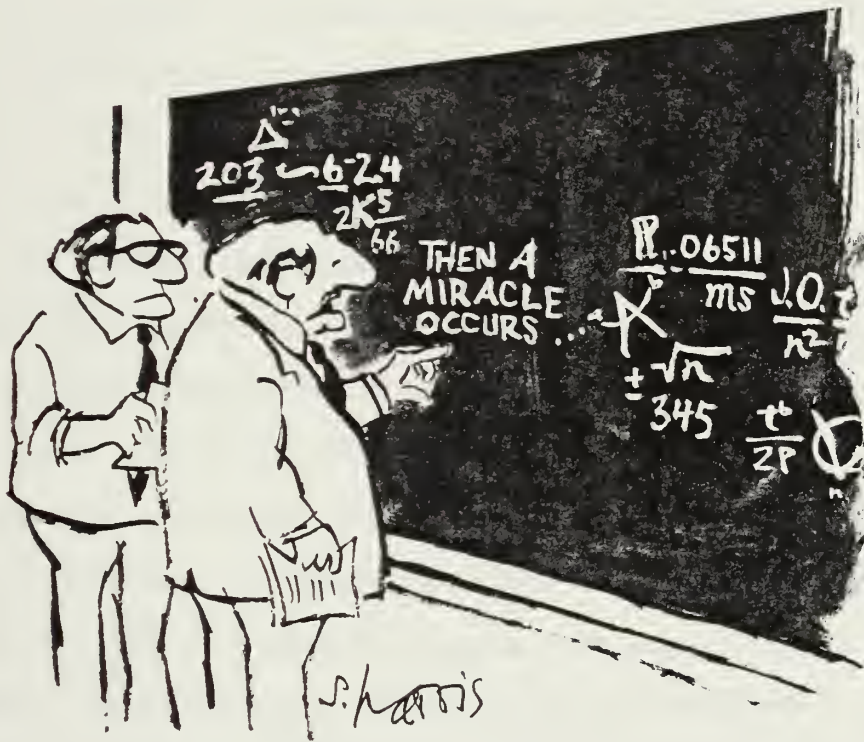
Computer Variables

DK	=	Reduced Frequency, k
DLAMDA	=	λ
DM2	=	m^2
DR	=	$mp = x_*$
ETA	=	η
ETASTR	=	η_*
IPT	=	Print Parameter
N	=	n
NF	=	not used
OFFSET	=	r
OMEGA	=	ω
QALPHA	=	$0 + i(\lambda - k)$
QCONST	=	$e^{i\sigma}$
QDCL	=	$C\ell_\alpha$
QDCM	=	Cm_α
QDK	=	$0 + ik$
QEXP	=	$0 + i\lambda$
QINTAP, QINTRP	=	Variables used to transmit boundary condition integrals
Q1ABCF, Q1RBCF	=	Interference coefficients for adjacent and reference blades
Q1COF	=	Right hand side vector in collocation solution
Q1INT	=	Known matrix of integrals in collocation solution
Q1RBP, Q1ABP	=	Not used
Q2CP	=	Not used
Q2EXP	=	$e^{-i\lambda x}$

Q2PT	=	Not used
RHO	=	vertical displacement
RHP	=	local input variable for rho
SIGMA	=	σ
TAU	=	τ
XASTN	=	Current x station in adjacent blade coordinates
XSTN	=	Current x station in reference blade coordinates

ACKNOWLEDGEMENT

I would like to thank Professor Max F. Platzer without whose infinite patience this thesis would not have been written.



"I think you should be more explicit here in step two."

Cartoon Reprinted from American Scientist, Vol. 65, No. 6, Nov-Dec 1977 with permission from Sidney Harris.

I. INTRODUCTION

The analysis of unsteady transonic flows in aircraft turbopropulsion is an area of intense current interest. Rising fuel prices and increasing thrust requirements both point toward the need of turbomachinery capable of performing well with transonic or supersonic internal flow. But, increased flow has increased both the costs and uncertainties of engine designs. Flutter problems have already become a major consideration in engine development. Problems unforeseen in earlier days of turbine engine production have caused long development delays, or forced acceptance of engines producing less than their initial design thrust. These uncertainties cannot be avoided when an attempt is made to extend the state of the art, but they can be reduced by extending the range of analytical modeling.

Such extension must now be done piecemeal. The three-dimensional flows in turbomachinery, including the simultaneous effects of boundary layers, rotation, finite blade thickness, spanwise Mach distributions, and shocks, are well beyond present capability. Perhaps one day complete analysis will be practical, but it is not today. The best that can be done now is to approach the problem from one aspect at a time. Flow through a two dimensional cascade has been a useful tool in this partial analysis.

This thesis was originally to have been an extension of the work of Elder [1] and Schlein [2] to the case of a staggered cascade. Their work, based on Teipel's [3] linearization of the unsteady transonic small perturbation equation, analyzed transonic flow through oscillating unstaggered cascades by use of the collocation method. While the problem was easy to state, it was difficult to solve. Both Elder and Schlein had encountered difficulty in employing the collocation method. Therefore, it was decided that verification of the basic collocation solution presented by Gorelov [4] using a different linearization would be a worthwhile goal in itself.

The following investigation presents a verification of the development in [4], along with numerical results and suggestions for further work.

II. UNSTEADY TRANSONIC FLOW THEORY

Considering inviscid flow only, the following four equations govern the aerodynamic flow problem at hand:

The equation of state

$$p = \rho RT \quad (\text{II-1})$$

and the equations for the conservation of

$$1. \text{ Mass: } \operatorname{div}(\rho \vec{v}) + \frac{\partial \rho}{\partial t} = 0 \quad (\text{II-2})$$

$$2. \text{ Momentum: } \frac{D\vec{v}}{Dt} + \frac{1}{\rho} \nabla p = 0 \quad (\text{II-3})$$

$$3. \text{ Energy: } \frac{DS}{Dt} = 0 \quad (\text{II-4})$$

where

\vec{v} = velocity

p = pressure

S = entropy

R = universal gas constant

T = temperature

t = time

ρ = density

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \frac{\partial}{\partial x} \frac{\partial x}{\partial t} + \frac{\partial}{\partial y} \frac{\partial y}{\partial t}$$

The analysis starts with a uniform flow from infinity. This flow has velocity U_0 parallel to the x-axis. This

formulation can be simplified by working with the total velocity potential, Φ , where

$$u = \frac{\partial \Phi}{\partial x} = \Phi_x = x \text{ component of velocity} = \frac{\partial x}{\partial t} \quad (\text{II-5})$$

$$v = \frac{\partial \Phi}{\partial y} = \Phi_y = y \text{ component of velocity} = \frac{\partial y}{\partial t} \quad (\text{II-6})$$

Thus, the initial uniform flow is represented by the uniform flow potential

$$\Phi_0 = U_0 x \quad (\text{II-7})$$

This notation may be applied to the conservation equations for mass and momentum. The equation for conservation of mass

$$\text{div}(\rho \vec{v}) + \frac{\partial \rho}{\partial t} = 0 \quad (\text{II-8})$$

becomes for two-dimensional unsteady flow

$$\begin{aligned} \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial \rho}{\partial t} &= 0 \\ \left[\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} \right] + \rho \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) &= 0 \end{aligned} \quad (\text{II-9})$$

but

$$\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} = \frac{D\rho}{Dt}$$

and

$$u = \phi_x \quad \text{and} \quad v = \phi_y$$

Thus

$$\frac{D\rho}{Dt} + \rho(\phi_{xx} + \phi_{yy}) = 0$$

and

$$\phi_{xx} + \phi_{yy} = -\frac{1}{\rho} \frac{D\rho}{Dt} \quad (\text{II-10})$$

The speed of sound is given by

$$a^2 = \frac{dp}{d\rho}$$

Thus

$$\frac{D\rho}{Dt} = \frac{d\rho}{dp} \cdot \frac{Dp}{Dt} = \frac{1}{a^2} \frac{Dp}{Dt}$$

Applying this to equation (II-10) yields

$$\phi_{xx} + \phi_{yy} = -\frac{1}{\rho a^2} \frac{Dp}{Dt} \quad (\text{II-11a})$$

$$\phi_{xx} + \phi_{yy} = -\frac{1}{\rho a^2} (u p_x + v p_y + p_t) \quad (\text{II-11b})$$

$$= -\frac{1}{\rho a^2} [(\nabla\phi) \cdot (\nabla p) + p_t] \quad (\text{II-11c})$$

where ∇ is the gradient operator, $P_x = \frac{\partial P}{\partial x}$, $P_y = \frac{\partial P}{\partial y}$, $P_t = \frac{\partial P}{\partial t}$.

Laying this aside for the moment, consider the momentum equation (II-3)

$$\frac{D\vec{v}}{Dt} + \frac{1}{\rho} \nabla p = 0$$

$$\frac{D\vec{v}}{Dt} = \frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v}$$

Thus

$$\rho \left[\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \right] = \nabla p \quad (\text{II-12})$$

$$\vec{v} = \nabla \phi$$

so

$$\frac{\partial \vec{v}}{\partial t} = \frac{\partial}{\partial t} (\nabla \phi) = \nabla \frac{\partial \phi}{\partial t} \quad (\text{II-13})$$

and

$$(\vec{v} \cdot \nabla) \vec{v} = \nabla \frac{v^2}{2} - \vec{v} \times (\nabla \times \vec{v})$$

where

$$v^2 = u^2 + v^2$$

$$= \vec{v} \cdot \vec{v}$$

For irrotational flow

$$\nabla \times \vec{v} = 0$$

thus

$$(\vec{v} \cdot \nabla) \vec{v} = \frac{\nabla v^2}{2} \quad (\text{II-14})$$

Thus

$$\frac{\nabla p}{\rho} + \nabla \left[\phi_t + \frac{v^2}{2} \right] = 0 \quad (\text{II-15})$$

which after integration along a streamline becomes

$$\int \frac{dp}{\rho} + \phi_t + \frac{v^2}{2} = F(t) \quad (\text{II-16})$$

For uniform flow from infinity $F(t) = \frac{1}{2} U_o^2$ and thus the final result is

$$\int \frac{dp}{\rho} + \phi_t + \frac{v^2}{2} = \frac{1}{2} U_o^2 \quad (\text{II-17})$$

Differentiation with respect to t gives

$$p_t = -\rho(\phi_{tt} + \frac{1}{2} \frac{\partial V^2}{\partial t}) \quad (\text{II-18})$$

From (II-3)

$$-\nabla p = \rho \frac{D\vec{v}}{Dt} \quad (\text{II-19})$$

Substitute (II-18) and (II-19) into (II-11c) to obtain

$$\phi_{xx} + \phi_{yy} = \frac{1}{a^2} [(\nabla\phi) \cdot \frac{D\vec{v}}{Dt} + \phi_{tt} + \frac{1}{2} \frac{\partial V^2}{\partial t}] \quad (\text{II-20})$$

This may be further simplified

$$\begin{aligned} \frac{D\vec{v}}{Dt} &= \frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \\ &= \frac{\partial \vec{v}}{\partial t} + \frac{1}{2} \nabla V^2 \end{aligned}$$

Hence

$$\phi_{xx} + \phi_{yy} = \frac{1}{a^2} [(\nabla\phi) \cdot (\frac{\partial \vec{v}}{\partial t} + \frac{1}{2} \nabla V^2) + \phi_{tt} + \frac{1}{2} \frac{\partial V^2}{\partial t}] \quad (\text{II-21})$$

Expanding terms

$$\begin{aligned} (\nabla\phi) \cdot (\frac{\partial \vec{v}}{\partial t}) &= \nabla\phi \cdot (\frac{\partial}{\partial t} \nabla\phi) = \phi_x \phi_{xt} + \phi_y \phi_{yt} \\ \nabla\phi \cdot \frac{\nabla V^2}{2} &= \frac{\phi_x^2 \phi_{xx}}{2} + \frac{\phi_y^2 \phi_{yy}}{2} + \frac{\phi_x \phi_y \phi_{xy}}{2} + \frac{\phi_y \phi_x \phi_{yx}}{2} \\ &= \frac{\phi_x^2 \phi_{xx}}{2} + \frac{\phi_y^2 \phi_{yy}}{2} + \frac{2\phi_x \phi_y \phi_{xy}}{2} \end{aligned}$$

$$\begin{aligned}
\frac{1}{2} \frac{\partial V^2}{\partial t} &= \frac{1}{2} \frac{\partial}{\partial t} [(\nabla \phi) \cdot (\nabla \phi)] \\
&= \frac{1}{2} [\phi_x \phi_{xt} + \phi_{xt} \phi_x + \phi_y \phi_{yt} + \phi_{yt} \phi_y] \\
&= \phi_x \phi_{xt} + \phi_y \phi_{yt}
\end{aligned}$$

The final result obtained by combining terms is

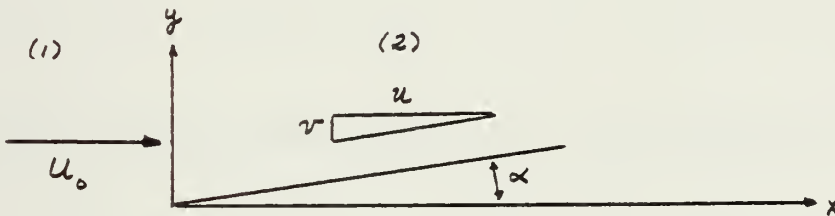
$$\begin{aligned}
\left(1 - \frac{\phi_x^2}{a^2}\right)_{xx} + \left(1 - \frac{\phi_y^2}{a^2}\right)_{yy} - \frac{2\phi_x \phi_y \phi_{xy}}{a^2} \\
- \frac{2\phi_x}{a^2} \phi_{xt} - \frac{2\phi_y}{a^2} \phi_{yt} - \frac{1}{a^2} \phi_{tt} = 0 \quad (\text{II-22})
\end{aligned}$$

This result is valid for irrotational, inviscid, two-dimensional, unsteady, compressible flows where gravity has been neglected.

III. SMALL PERTURBATION THEORY OF TRANSONIC FLOW

A. GENERAL CASE

A thin body at a small angle of attack will cause only a slight disturbance in the fluid. A flat plate is an example. Consider flow past a flat plate at angle of attack; α .



The flow at (2) must be parallel to the plate. To achieve this, small disturbance velocities u' and v' must be added to the free stream velocity yielding

$$u = U_0 + u'$$

$$v = v'$$

The potential of the disturbed flow may be considered as the sum of the uniform flow potential, $\phi_0 = U_0 x$, and the disturbance potential, ϕ

$$\phi = \phi_0 + \phi \quad (\text{III-1})$$

Thus

$$\phi_x = U_o + u' \quad (\text{III-2a})$$

$$\phi_y = v \quad (\text{III-2b})$$

If ϕ is a function of time, then

$$\phi_t = \phi_t$$

This result may be substituted into (II-22) leading to

$$\begin{aligned} & \left[1 - \frac{(U_o + u')^2}{a^2}\right] \phi_{xx} + \left[1 - \frac{v^2}{a^2}\right] \phi_{yy} - 2 \frac{(U_o + u')v}{a^2} \phi_{xy} \\ & - 2 \frac{(U_o + u')}{a^2} \phi_{xt} - \frac{2v}{a^2} \phi_{yt} - \frac{1}{a^2} \phi_{tt} = 0 \quad (\text{III-3}) \end{aligned}$$

This expands to yield

$$\begin{aligned} & \left[1 - \frac{U_o^2 + 2U_o u' + u'^2}{a^2}\right] \phi_{xx} + \left[1 - \frac{v^2}{a^2}\right] \phi_{yy} - 2 \frac{(U_o v + u' v)}{a^2} \phi_{xy} \\ & - 2 \frac{(U_o + u')}{a^2} \phi_{xt} - \frac{2v}{a^2} \phi_{yt} - \frac{1}{a^2} \phi_{tt} = 0 \quad (\text{III-4}) \end{aligned}$$

Equation (III-4) may be further simplified as shown by Landahl [3]. All non-linear terms except the $\phi_x \phi_{xx}$ product

term can be neglected yielding the following transonic small disturbance equation

$$[(M^2-1) + (\gamma+1)M^2 \frac{\phi_x}{U_0}] \phi_{xx} - \phi_{yy} + \frac{2M_0}{a_0} \phi_{xt} + \frac{1}{a_0} \phi_{tt} = 0 \quad (\text{III-5})$$

where a_0 is the velocity of sound in the free-stream, and γ is the ratio of specific heats, and $M_0 = \text{Mach number}$.

B. BOUNDARY CONDITION

The tangential flow condition requires that the flow be tangent to the airfoil surface at each instant of time. This means that no fluid may flow through the surface of the airfoil and is expressed by the condition

$$\frac{DG}{Dt} = 0 \quad \text{on } G(x,y,t) \quad (\text{III-6})$$

where

$G(x,y,t)$ describes the surface of the body as a function of time.

For a thin airfoil restricted to small oscillations, this may be written as

$$G = y - H(x,t) \quad (\text{III-7})$$

where

$H(x,t)$ is the function describing the position of the airfoil.

$H(x,t)$ can be written for harmonic pitch oscillations as

$$H(x,t) = \text{R.P.}[\alpha_0(x-x_0) e^{i\nu t}] \quad (\text{III-8})$$

where the time-varying angle of attack $\alpha(t)$ is given by

$$\alpha(t) = \text{R.P.}[\alpha_0 e^{i\nu t}]$$

and α_0 = maximum amplitude of pitch oscillation

x_0 is the pitch axis

ν is the angular frequency of oscillation

$$i = \sqrt{-1}$$

R.P. = "real part of"

Inserting (III-8) into the flow tangency condition (III-6) gives, after linearization,

$$\phi_y(x,0) = v(x,0) = \alpha_0[U_0 + i\nu(x - x_0)] e^{i\nu t} \quad (\text{III-9})$$

on $y = 0$

This is a condition for the normal velocity to be prescribed at the airfoil's mean position $y = 0$.

C. NONDIMENSIONALIZATION

The terms in equations (III-5) and (III-9) are dimensional. For the following calculations it is convenient to use non-dimensional quantities. Define non-dimensional time and length to be

$$\bar{x} = \frac{x}{c}$$

$$\bar{y} = \frac{y}{c} \quad (\text{III-10})$$

$$\bar{t} = \frac{tU_o}{c}$$

where

U_o = uniform velocity from infinity

c = reference length (blade semichord).

The velocity potential in equation (III-5) may be non-dimensionalized as follows. Let

$$\bar{\phi} = \frac{\phi}{U_o c}$$

Hence:

$$\phi = U_o c \bar{\phi}$$

$$\phi_x = U_o c \bar{\phi}_{\bar{x}} \left(\frac{1}{c} \right)$$

$$= U_o \bar{\phi}_{\bar{x}} \quad (\text{III-11})$$

and similarly for the other derivatives in (III-5), yielding

$$[(M^2-1) + (\gamma+1)M^2\bar{\phi}_x] \phi_{\bar{x}\bar{x}} - \bar{\phi}_{\bar{y}\bar{y}} + 2M^2\bar{\phi}_{\bar{x}\bar{t}} + M^2\bar{\phi}_{\bar{t}\bar{t}} = 0$$

(III-12)

This equation is non-dimensional.

The boundary condition given in equation (III-9) may be non-dimensionalized in a similar fashion

$$\phi_y(x,0) = \alpha_o [U_o + i\nu(x - x_o)] e^{i\nu t} \quad (\text{III-9})$$

Thus

$$U_o c \bar{\phi}_y = \alpha_o [U_o + ik \frac{U_o}{c} (c\bar{x} - c\bar{x}_o)] e^{i\nu \bar{t} \frac{c}{U_o}} \quad (\text{III-13})$$

where

$$k = \frac{\nu c}{U_o} = \text{Strouhal number or reduced frequency}$$

$$U_o c \bar{\phi}_y \cdot \frac{1}{c} = \alpha_o U_o [1 + ik(\bar{x} - \bar{x}_o)] e^{ik\bar{t}} \quad (\text{III-14})$$

Thus

$$\bar{\phi}_y = \bar{v}(\bar{x},0) = \alpha_o [1 + ik(\bar{x} - \bar{x}_o)] e^{ik\bar{t}} \quad (\text{III-15})$$

Because the final operations are linear in α_o , set $\alpha_o = 1$, yielding

$$\bar{\phi}_y = \bar{v}(\bar{x},0) = [1 + ik(\bar{x} - \bar{x}_o)] e^{ik\bar{t}} \quad (\text{III-16})$$

The overbars denoting nondimensional quantities will be dropped from the remainder of the paper. All further quantities shall be assumed appropriately non-dimensional. This yields the following final equations

$$[(M^2-1)+(\gamma+1)M^2]\phi_{xx} - \phi_{yy} + 2M^2\phi_{xt} + M^2\phi_{tt} = 0 \quad (\text{III-17})$$

and

$$\phi_y(x,0) = v(x,0) = [1 + ik(x - x_0)] e^{ikt} \quad (\text{III-18})$$

where

all quantities are nondimensional and

$$\alpha_0 = 1$$

D. HARMONIC OSCILLATIONS

In the case of harmonic oscillations, equation (III-17) may be simplified still further.

Let

$$\phi = \tilde{\phi} + \text{R.P.}[\psi e^{ikt}]$$

where

$\tilde{\phi}$ = non-dimensional steady flow potential

ψ = non-dimensional oscillatory flow potential

R.P. = "real part of"

Equation (III-17) then becomes

$$\begin{aligned}
 (1-M^2)\psi_{xx} + \psi_{yy} - M^2(\gamma+1)[\psi_x\psi_{xx} + \tilde{\phi}_x\psi_{xx} + \tilde{\phi}_{xx}\psi_x] \\
 + M^2k^2\psi - 2iMk^2\psi_x = 0
 \end{aligned}
 \tag{III-19}$$

For M close to 1, this is a nonlinear mixed elliptic-hyperbolic partial differential equation with variable coefficients, the exact type depending on $\tilde{\phi}_x$ and $\tilde{\phi}_{xx}$. However, because flutter analysis is primarily concerned with the stability of small perturbations about a steady flow, the oscillatory component may be assumed small compared to the steady flow potential and therefore the product term $\psi_x\psi_{xx}$ may be neglected, yielding,

$$\begin{aligned}
 (1-M^2)\psi_{xx} + \psi_{yy} - M^2(\gamma+1)[\tilde{\phi}_x\psi_{xx} + \tilde{\phi}_{xx}\psi_x] \\
 = 2iM^2k\psi_x + M^2k^2\psi = 0
 \end{aligned}
 \tag{III-20}$$

IV. LINEARIZATION OF THE GOVERNING EQUATION

The basic flutter equation, (III-20), is still a non-linear, mixed elliptic-hyperbolic partial differential equation with variable coefficients and difficult to solve. It may yet be further simplified.

A. BASIC SOLUTION

For $M = 1$, equation (III-20) becomes

$$\psi_{YY} - (\gamma+1)[\tilde{\phi}_x \psi_{xx} + \tilde{\phi}_{xx} \psi_x] - 2ik\psi_x + k^2\psi = 0 \quad (\text{IV-1})$$

Now assume

$$\tilde{\phi}_x \approx w = \text{constant} \quad (\text{IV-2})$$

$$\tilde{\phi}_{xx} \approx 0$$

throughout the interblade channel. Setting

$$\tilde{\phi}_x(\gamma+1) = w(\gamma+1) = m^2 \quad (\text{IV-3})$$

yields

$$m^2\psi_{xx} - \psi_{YY} + 2ik\psi_x - k^2\psi = 0 \quad (\text{IV-4})$$

The solution to this equation is found in Garrick and Rubinow [5]

$$\psi(x,y) = -\frac{1}{m} \int_{x_\ell}^{x-my} v(s) J_0[\omega \sqrt{(x-s)^2 - (my)^2}] e^{i\lambda(s-x)} ds \quad \text{for } y > 0 \quad (\text{IV-5a})$$

and

$$\psi(x,y) = \frac{1}{m} \int_{x_\ell}^{x+my} v(s) J_0[\omega \sqrt{(x-s)^2 - (my)^2}] e^{i\lambda(s-x)} dx \quad \text{for } y < 0 \quad (\text{IV-5b})$$

where

$$v(x) = \lim_{y \rightarrow 0} \frac{\partial}{\partial y} \psi(x,y) .$$

$v(x)$ may be obtained directly from the tangential flow boundary condition, and

$$\omega = \frac{k^2(1-m^2)}{m^4}$$

$$\lambda = \frac{k}{m^2} \sqrt{1+m^2} \approx \frac{k}{m^2} \quad \text{(where this paper employs the approximation used by Gorelov [4])}$$

$$x_\ell = \text{blade leading edge,}$$

Gorelov [4], has proposed a further simplification.

Set

$$z = my \quad (\text{IV-6a})$$

$$\Psi(x, z) = \psi(x, y) e^{i\lambda x} \quad (\text{IV-6b})$$

Equation (IV-4) then becomes

$$\Psi_{xx} - \Psi_{zz} + \omega^2 \Psi = 0$$

with solution

$$\Psi(x, z) = -\frac{1}{m} \int_{x_\ell}^{x-z} v(s) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds \quad (\text{IV-7a})$$

$$z > 0$$

$$\Psi(x, z) = \frac{1}{m} \int_{x_\ell}^{x-z} v(s) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds \quad (\text{IV-7b})$$

$$z < 0$$

where

$$v(x) = me^{-i\lambda x} \lim_{z \rightarrow 0} \Psi_z(x, z)$$

$v(x)$ is obtained from the tangential flow boundary condition.

For a thin body immersed in the flow, the solutions for $y > 0$, $z > 0$, and $y < 0$, $z < 0$ apply above the body along left-running Mach lines, or below along right running Mach lines respectively.

B. BOUNDARY CONDITIONS

1. Flow Tangency Condition

The boundary condition comes from the tangential flow condition, (III-18)

$$v(x) = [1 + ik(x - x_0)] \quad (\text{IV-8})$$

2. Upstream Condition

The final linearized equation is a hyperbolic differential equation with boundary condition

$$\psi(x, y) = 0 \quad (\text{IV-9})$$

when

$$x - x_\ell < |my|$$

for the solution shown in equations (IV-5) or

$$\Psi(x, z) = 0$$

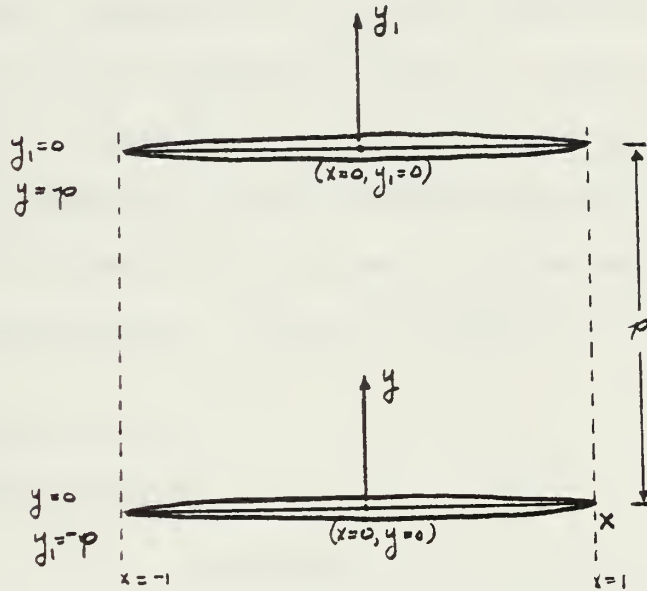
when

$$x - x_{\ell} < |z|$$

for the solution shown in equations (IV-7).

V. PROBLEM FORMULATION

A. CO-ORDINATE SYSTEM



Assume the geometry shown above. Both blades are thin airfoils of semichord c . All measurements are non-dimensional, normalized to c . The (x, y) co-ordinate system has its origin at the center of the reference (lower) blade. The (x, y_1) system is centered at the middle of the adjacent (upper) blade. The origin of the (x, y_1) system is located at $(0, p)$ in the reference system. Generalizing this convention, the same symbols shall be used for the same quantities on both blades. Where discrimination is required, the quantity associated with the adjacent blade will be marked with

superscript ¹, the quantity associated with the reference blade will be either unsuperscripted or marked with a superscript ⁰.

Each blade is assumed to perform a small amplitude harmonic oscillation about its mid-chord point. Both blades are assumed to have identical reduced frequencies, k , and the motion of the adjacent blade lags that of the reference blade by a phase angle σ .

The blades are immersed in a uniform flow from the left at $M = 1$. The objective is to determine the oscillatory pressure distributions and aerodynamic forces generated by the blades' oscillations. Cascade solidity, $\tau = 2/p$.

B. BOUNDARY CONDITIONS

1. Upstream Condition

$$\begin{aligned} \psi &= 0 && \text{whenever} \\ x + 1 &< |my| && (V-1) \\ &\text{and} \\ x + 1 &< |my_1|, && \text{simultaneously} \end{aligned}$$

2. Flow Tangency Condition

Along the reference blade

$$\lim_{y \rightarrow 0} \psi_y(x, y) = (1 + ikx) \quad (V-2a)$$

Along the adjacent blade

$$\lim_{y_1 \rightarrow 0} \psi_{y_1}(x, y_1) = (1 + ikx)e^{i\sigma} \quad (V-2b)$$

where

σ is the phase angle between the blades oscillations

C. BASIC SOLUTION TECHNIQUE

Assume that the unsteady potential, ψ , may be written as the sum of four components

$$\psi(x, y) = \phi^0(x, y) + \psi^0(x, y) + \phi^1(x, y_1) + \psi^1(x, y_1) \quad (V-3)$$

where:

- ϕ^0 = potential due to the reference blade alone, known from equation (IV-7)
- ϕ^1 = potential due to the adjacent blade alone, known from equation (IV-7)
- ψ^0 = interference potential required to satisfy tangential flow condition along reference blade, unknown
- ψ^1 = interference potential required to satisfy tangential flow condition along adjacent blade, unknown.

This total potential must satisfy the tangential flow condition at the plane of both the reference and adjacent blades. Thus

$$\begin{aligned} \phi_Y^0(x, y=0) + \phi_{y_1}^1(x, y_1=-p) + \psi_Y^0(x, y=0) + \psi_{y_1}^1(x, y_1=-p) \\ = (1 + ikx) \end{aligned} \quad (V-4a)$$

at the reference blade, and

$$\begin{aligned} \phi^0(x, y=p) + \phi_{Y_1}^1(x, y_1=0) + \psi_Y^0(x, y=p) + \psi_{Y_1}^1(x, y_1=0) \\ = (1 + ikx) e^{i\sigma} \end{aligned} \quad (V-4b)$$

at the adjacent blade.

But from the unsteady potential solution for a single oscillating blade one has

$$\phi_Y^0(x, y=0) = 1 + ikx \quad (V-5a)$$

and

$$\phi_{Y_1}^1(x, y_1=0) = (1 + ikx) e^{i\sigma} \quad (V-5b)$$

Thus

$$\phi_{Y_1}^1(x, y_1=-p) + \psi_{Y_1}^1(x, y_1=-p) + \psi_Y^0(x, y=0) = 0 \quad (V-6a)$$

along the reference blade, and

$$\phi_Y^0(x, y=p) + \psi_Y^0(x, y=p) + \psi_{Y_1}^1(x, y_1=0) = 0 \quad (V-6b)$$

along the adjacent blade.

From equation (IV-7)

$$\phi^0(x, y) = -\frac{1}{m} \int_{-1}^{x-my} v^0(s) J_0[\omega \sqrt{(x-s)^2 - (my)^2}] e^{i\lambda(s-x)} ds$$

$$y > 0 \quad (V-7a)$$

$$= \frac{1}{m} \int_{-1}^{x+my} v^0(s) J_0[\omega \sqrt{(x-s)^2 - (my)^2}] e^{i\lambda(s-x)} ds$$

$$y < 0 \quad (V-7b)$$

where

$$v^0(s) = 1 + iks$$

$$\lambda = k/m^2$$

$$m = (\gamma+1)w$$

$$\omega = \frac{k^2(1-m^2)}{m^4}$$

$$w = \text{mean value of } \tilde{\phi}_x \text{ in the channel}$$

$$\phi^1(x, y_1) = -\frac{1}{m} \int_{-1}^{x-my_1} v^1(s) J_0[\omega \sqrt{(x-s)^2 - (my_1)^2}] e^{i\lambda(s-x)} ds$$

$$y_1 > 0 \quad (IV-8a)$$

$$= \frac{1}{m} \int_{-1}^{x+my_1} v^1(s) J_0[\omega \sqrt{(x-s)^2 - (my_1)^2}] e^{i\lambda(s-x)} ds$$

$$y_1 < 0 \quad (IV-8b)$$

where

$$v^1(s) = (1 + iks)e^{i\sigma}$$

Henceforth attention will be restricted to the flow within the channel, $0 \leq y \leq p$, $-p \leq y_1 \leq 0$ leaving (IV-7a) and (IV-8b) as the governing equations of interest.

The two interference potentials are assumed to have forms identical to (IV-7a) and (IV-8b).

Set

$$\psi^0(x, y) = -\frac{1}{m} \int_{-1}^{x-my} u^0(s) J_0[\omega \sqrt{(x-s)^2 - (my)^2}] e^{i\lambda(s-x)} ds$$

(V-9a)

$y > 0$

$$\psi^1(x, y_1) = \frac{1}{m} \int_{-1}^{x+m} u^1(s) J_0[\omega \sqrt{(x-s)^2 - (my_1)^2}] e^{i\lambda(s-x)} ds$$

(V-9b)

$y_1 < 0$

where

$u^0(s)$ and $u^1(s)$ are unknown functions to be determined so as to satisfy equations (V-6)

Substitution of (V-7a), (V-8b) and (V-9) into (V-6) yields

$$u^0(x) + \psi_{y_1}^1(x, y_1 = -p) + \phi_{y_1}^0(x, y_1 = -p) = 0 \quad (V-10a)$$

$$u^1(x) + \psi_Y^0(x, y=p) + \phi_Y^0(x, y=p) = 0 \quad (V-10b)$$

Recalling Gorelov's transformation discussed in [4] and shown in equations (IV-6) above, set

$$\phi^0(x, z) = \phi^0(x, y) e^{i\lambda x}$$

$$\phi^1(x, z_1) = \phi^1(x, y_1) e^{i\lambda x}$$

$$\psi^0(x, z) = \psi^0(x, y) e^{i\lambda x}$$

$$\psi^1(x, z_1) = \psi^1(x, y_1) e^{i\lambda x}$$

where $z = my$

$$z_1 = my_1$$

Then

$$\frac{e^{i\lambda x}}{m} u^0(x) + \phi_{z_1}^1(x, z_1 = -x_*) + \psi_{z_1}^1(x, z_1 = -x_*) = 0 \quad (V-11a)$$

and

$$\frac{e^{i\lambda x}}{m} u^1(x) + \phi_z^0(x, z = x_*) + \psi_z^0(x, z = x_*) = 0 \quad (V-11b)$$

where

$$x_* = mp.$$

To employ the collocation method, assume that $u^1(x)$ and $u^0(x)$ can be approximated as the sum of a set of elementary functions f_j so that

$$u^0(x) \approx \sum_{j=0}^n \theta_j^0 f_j(x) \quad (V-12a)$$

$$u^1(x) \approx \sum_{j=0}^n \theta_j^1 f_j(x) \quad (V-12b)$$

where $f_j(x) = 0$ when $x \leq x_* - 1$

Note that here both u^0 and u^1 are expressed in terms of the same elementary functions, f_j .

Because of the slightly supersonic nature of the problem observe that $u^0(x) = 0$ and $u^1(x) = 0$ when $x \leq x_* - 1$.

Equations (V-12) may now be rewritten as

$$\begin{aligned} e^{i\lambda x} \sum \theta_j^0 f_j(x) + \frac{\partial}{\partial z_1} \int_{x_*-1}^{x+z_1} \sum \theta_j^1 f_j(s) J_0[\omega \sqrt{(x-s)^2 - z_1^2}] e^{i\lambda s} ds \\ = -e^{i\sigma} \frac{\partial}{\partial z_1} \int_{-1}^{x+z_1} (1+iks) J_0[\omega \sqrt{(x-s)^2 - z_1^2}] e^{i\lambda s} ds \end{aligned}$$

at $z_1 = -x_*$ (V-13a)

$$\begin{aligned}
e^{i\lambda x} \sum_j \theta_j^1 f_j(x) - \frac{\partial}{\partial z} \int_{x_*-1}^{x-z} \sum_j \theta_j^0 f_j(s) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds \\
= \frac{\partial}{\partial z} \int_{-1}^{x+z} (1+iks) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds
\end{aligned}$$

$$\text{at } z = x_* \quad (V-13b)$$

where

$$f_j(x) = 0 \text{ for } x \leq x_* - 1$$

This simplifies to

$$\begin{aligned}
e^{i\lambda x} \sum_j \theta_j^0 f_j(x) + \sum_j \theta_j^1 \left\{ \frac{\partial}{\partial z_1} \int_{x_*-1}^{x+z_1} f_j(s) J_0[\omega \sqrt{(x-s)^2 - z_1^2}] e^{i\lambda s} ds \right\} \\
= -e^{i\sigma} \frac{\partial}{\partial z_1} \int_{-1}^{x+z_1} (1+iks) J_0[\omega \sqrt{(x-s)^2 - z_1^2}] e^{i\lambda s} ds
\end{aligned}$$

$$\text{at } z_1 = -x_* \quad (V-14a)$$

and

$$\begin{aligned}
e^{i\lambda x} \sum_j \theta_j^1 f_j(x) - \sum_j \theta_j^0 \left\{ \frac{\partial}{\partial z} \int_{x_*-1}^{x-z} f_j(s) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds \right\} \\
= \frac{\partial}{\partial z} \int_{-1}^{x-z} (1+iks) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds \quad (V-14b)
\end{aligned}$$

at $z = x_*$ where

$$f_j(x) = 0 \text{ for } x \leq x_* - 1.$$

Performing the indicated differentiation yields

$$\begin{aligned} & e^{i\lambda x} \left\{ \theta_j^0 f_j(x) + \left[\theta_j^1 \left\{ \int_{x_*-1}^{x-x_*} f_j(s) \frac{J_1[\omega \sqrt{(x-s)^2 - x_*^2}] \omega x_* e^{i\lambda s} ds}{\sqrt{(x-s)^2 - x_*^2}} \right. \right. \right. \\ & \quad \left. \left. \left. + f_j(x-x_*) e^{i\lambda(x-x_*)} \right\} \right] \right\} \\ & = e^{i\sigma} \left\{ - \int_{-1}^{x-x_*} (1+iks) \frac{\omega x_* J_1[\omega \sqrt{(x-s)^2 - x_*^2}] e^{i\lambda s} ds}{\sqrt{(x-s)^2 - x_*^2}} \right. \\ & \quad \left. - [1+ik(x-x_*)] e^{i\lambda(x-x_*)} \right\} \end{aligned} \quad (V-15a)$$

and

$$\begin{aligned} & e^{i\lambda x} \left\{ \theta_j^1 f_j(x) + \left[\theta_j^0 \left\{ \int_{x_*-1}^{x-x_*} f_j(s) \frac{J_1[\omega \sqrt{(x-s)^2 - x_*^2}] \omega x_* e^{i\lambda s} ds}{\sqrt{(x-s)^2 - x_*^2}} \right. \right. \right. \\ & \quad \left. \left. \left. + f_j(x-x_*) e^{i\lambda(x-x_*)} \right\} \right] \right\} \\ & = - \int_{-1}^{x-x_*} (1+iks) \frac{\omega x_* J_1[\omega \sqrt{(x-s)^2 - x_*^2}] e^{i\lambda s} ds}{\sqrt{(x-s)^2 - x_*^2}} - [1+ik(x-x_*)] e^{i\lambda(x-x_*)} \end{aligned} \quad (V-15b)$$

Gorelov's formulation, equations [2.6, 2.7, 2.8, and 2.9] of [4], can be obtained directly from equations (V-15) by substituting

$$f_j(x) = \cos j\eta - \cos j\eta_*$$

$$v^0 = \sum_{j=0}^n \mu_j^0 \cos j\eta$$

$$v^1 = \sum_{j=0}^n \mu_j^1 \cos j\eta$$

where:

$$\eta = \cos(-x)$$

$$\eta_* = \cos(1-x_*)$$

In comparing the two systems care must be taken to note the differing symbols and coordinate systems. The corresponding quantities are:

Here	in[4]
θ_j^0, θ_j^1	$v_{0\sigma}, v_{i\sigma}$
μ_j^0, μ_j^1	$\theta_{0\sigma}, \theta_{i\sigma}$
$\eta = \cos^{-1}(-x)$	$\eta = \cos^{-1}(1-x)$
$\eta_* = \cos^{-1}(1-x_*)$	$\eta_* = \cos^{-1}(1-x_*)$
z, z_1	Y, Y_1
j	σ
σ	ψ

Here $-1 \leq x \leq 1$; in [4] $0 \leq x \leq 2$. This transformation accounts for the differing definitions of η . Making the substitutions results in the system

n

$$\sum_{j=0} \{ \theta_j^0 [\cos j\eta - (1-\delta_{01}) \cos j\eta_*] \}$$

$$+ \theta_j^1 \int_{x_*-1}^{x-x_*} \frac{\partial}{\partial z_1} J_0 [\omega \sqrt{(x-s)^2 - z_1^2}] [\cos j\hat{\eta} - (1-\delta_{i0}) \cos j\eta_*] e^{i\lambda s} ds$$

$$+ \theta_i^1 [\cos j\bar{\eta} - (1-\delta_{i0}) \cos j\eta_*] e^{i\lambda(x-x_*)} \}$$

$$= - \sum_{j=0}^n \{ -\mu_j^1 \int_{-1}^{x-x_*} \frac{\partial}{\partial z_1} J_0 [\sqrt{(x-s)^2 - z_1^2}] \cos j\hat{\eta} e^{i\lambda s} ds$$

$$- \mu_j^1 \cos j\bar{\eta} e^{i\lambda(x-x_*)} \} \quad (V-16a)$$

$$\text{at } z_1 = -x_*$$

$$x > x_* - 1$$

and

$$\sum \{ \theta_j^1 [\cos j\eta - (1-\delta_{oj}) \cos j\eta_*] \}$$

$$+ \theta_j^0 \int_{x_*-1}^{x-x_*} \frac{\partial}{\partial z} J_0 [\omega \sqrt{(x-s)^2 - z^2}] [\cos j\eta - (1-\delta_{oj}) \cos j\eta_*] e^{i\lambda s} ds$$

$$+ \theta_j^0 [\cos j\bar{\eta} - (1-\delta_{oj}) \cos j\eta_*] e^{i\lambda(x-x_*)} \}$$

$$= \sum_{j=0}^n \{ \mu_j^0 \int_{-1}^{x-x_*} \frac{\partial}{\partial z} J_0 [\omega \sqrt{(x-s)^2 - z^2}] \cos j\hat{\eta} e^{i\lambda s} ds$$

$$- u_j^0 \cos j\bar{\eta} e^{i\lambda(x-x_*)} \} \quad (V-16b)$$

where:

$$\eta = \arccos(-x)$$

$$\eta_* = \arccos(1-x_*)$$

$$\bar{\eta} = \arccos(-s)$$

$$\hat{\eta} = \arccos(-x+x_*)$$

$$\delta_{\bar{o}j} = \text{Dirac } \delta \text{ function} = \begin{matrix} 1 & \text{for } j = 0 \\ 0 & \text{for } j \neq 0 \end{matrix}$$

Given the change in coordinates and notation, this system is equivalent to that shown in [4].

This was the system programmed for computer solution. Because the function, $f_j(x)$, is unaffected by the differentiation with respect to y (or z) the exact form used need not be specified, so that the system shown in (V-15) may be programmed with f undetermined. A subroutine may be written to return the function desired and the remaining program left perfectly general. In the program developed with this thesis both the Gorelov functions shown above and the Legendre polynomials were employed. All the integrals may now be evaluated at $n+1$ points, x_i , on both blades in $mp-1 < x_i < 1$ and the resulting linear system solved for θ_j^0 and θ_j^1 , $j=1,2,\dots,n+1$.

The interference potentials may be constructed by taking

$$\psi^0(x,z) = \frac{-1}{m} \int_1^{x-z} [\theta_j^0 f_j(x)] J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds$$

$$z > 0 \quad (V-17a)$$

$$\psi^1(x,z_1) = \frac{1}{m} \int_{-1}^{x+z_1} [\theta_j^1 f_j(x)] J_0[\omega \sqrt{(x-s)^2 - z_1^2}] e^{i\lambda s} ds$$

$$z_1 < 0 \quad (V-17b)$$

where

$$f_j(x) = 0, \quad \text{for all } x \leq x_* - 1$$

Once the potentials have been calculated as outlined above, the surface pressure may be calculated using the relationship

$$C_p = -2(\psi_x + ik\psi) \quad (V-18a)$$

$$= -2[\Psi_x + i(k-\lambda)\Psi]e^{-i\lambda x} \quad (V-18b)$$

Because all the plates are assumed to be in steady oscillation with uniform phase shift, σ , between neighboring plates, then

$$v^1(x) = v^0(x)e^{i\sigma}, \quad u^1(x) = u^0(x)e^{i\sigma}, \quad \Psi(x,y) = -\Psi(x,-y)$$

in this case

$$C_{\ell\alpha} = 2 \int_{-1}^1 [\Psi_x(x,+0) + i(k-\lambda)\Psi(x,+0)]e^{-i\lambda x} dx \quad (V-19)$$

where

$$\begin{aligned} \Psi(x_1,+0) &= \frac{-1}{m} \int_{-1}^x [(1+iks)+u^0(s)]J_0[\omega(x-s)]e^{i\lambda(s)} ds \\ &+ \frac{e^{i\sigma}}{m} \int_{-1}^{x-x_*} [(1+iks)+u^0(s)]J_0[\omega\sqrt{(x-s)^2-(x_*)^2}]e^{i\lambda(s)} ds \end{aligned}$$

where $x_* = mp.$ (V-20)

Results from this approach, in the form of values of $C_{\ell\alpha}$ for $k = 0.1$, at various values of w are presented in the results for

approximations based both on Gorelov's formulation, and on the Legendre polynomials.

D. COLLOCATION SOLUTION OF THE POTENTIAL EQUATION EXPANDED FOR SMALL k ,

In order to provide a partially independent check of the results of the main program, the Gorelov function representation of the collocation solution was expanded for small k , and solved at two collocation points, $n = 2$. The resulting potentials, and partial derivatives with respect to x and y were then used to replace the corresponding numerical routines in the main program. The output resulting from the approximations were compared with the purely numerical results obtained from the computer program.

1. Solution For The Unknown Potential Coefficients

The basic system of linear equations used to determine the unknown coefficients is

$$\frac{1}{m} e^{i\lambda x} u^0 + \phi_{z_1}^1 + \psi_{z_1}^1 = 0, \quad z = 0, \quad z_1 = -x_* = -mp \quad (V-21a)$$

$$\frac{1}{m} e^{i\lambda x} u^1 + \phi_z^0 + \psi_z^0 = 0, \quad z_1 = 0, \quad z = x_* = mp \quad (V-21b)$$

where

$$0 = u^0(x) = u^1(x) \quad \text{when} \quad x \leq -1+x_*$$

otherwise

$$u^0 = \sum_{j=1}^n \theta_j^0 (\cos j\eta - \cos j\eta_*) + \theta_0^0$$

$$u^1 = \sum_{j=1}^n \theta_j^1 (\cos j\eta - \cos j\eta_*) + \theta_0^1$$

where

$$\eta = \arccos(-x)$$

$$\eta_* = \arccos(1 - x_*)$$

Thus, for $n = 2$, the system becomes

$$e^{i\lambda x} \{ \theta_0^0 + \theta_1^0 (\cos \eta - \cos \eta_*) \}$$

$$+ \frac{\partial}{\partial z_1} \int_{-1}^{x+z_1} v^1(s) J_0 [\omega \sqrt{(x-s)^2 - z_1^2}] e^{i\lambda s} ds$$

$$+ \frac{\partial}{\partial z_1} \int_{x_*-1}^{x+z_1} u^1(s) J_0 [\omega \sqrt{(x-s)^2 - z_1^2}] e^{i\lambda s} ds = 0$$

$$z_1 = -x_* \quad (V-22a)$$

along the reference blade and

$$e^{i\lambda x} \{ \theta_0^1 + \theta_1^1 (\cos \eta - \cos \eta_*) \} - \frac{\partial}{\partial z} \int_{-1}^{x-z} v^0(s) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds$$

$$- \frac{\partial}{\partial z} \int_{x_*-1}^{x-z} u^0(s) J_0[\omega \sqrt{(x-s)^2 - z^2}] e^{i\lambda s} ds \quad (V-22b)$$

$$z = x_*$$

along the adjacent blade

$$\text{where} \quad u^0(s) = \theta_0^0 + \theta_1^0 (\cos \eta - \cos \eta_*)$$

$$u^1(s) = \theta_0^1 + \theta_1^1 (\cos \eta - \cos \eta_*)$$

$$v^0(s) = 1 + iks$$

$$v^1(s) = (1 + iks) e^{i\sigma}$$

For k sufficiently small, this system may be further simplified by the following approximations

$$J_0[\omega \sqrt{(x-s)^2 - z^2}] \approx 1 - O(\omega^2) \approx 1 \quad (V-23a)$$

$$J_0[\omega \sqrt{(x-s)^2 - z^2}] \approx 1 - O(\omega^2) \approx 1 \quad (V-23b)$$

$$e^{i\lambda x} \approx 1 + i\lambda x - O(\lambda^2 x^2) \approx 1 + i\lambda x$$

$$e^{i\lambda s} \approx 1 + i\lambda s - O(\lambda^2 s^2) \approx 1 + i\lambda s$$

where $O(\omega^2)$ means "of the order of magnitude of ω^2 "

$$-1 \leq x \leq 1, \quad -1 \leq s \leq x - x_*$$

$$\lambda = k/m^2, \quad \omega^2 = \frac{k^2(1-m^2)}{m^4}$$

The interference source distributions may be replaced by

$$u^0(s) = \theta_0^0 + \theta_1^0(-s + x_* - 1)$$

$$u^1(s) = \theta_0^1 + \theta_1^1(-s + x_* - 1) .$$

If higher order terms are neglected, the result is a system linear in k and λ

$$\begin{aligned} (1+i\lambda x) [\theta_0^0 + \theta_1^0(-x-1+x_*)] + \frac{\partial e^{i\sigma}}{\partial z_1} \int_{-1}^{x+z_1} (1+iks)(1+i\lambda s) ds \\ + \frac{\partial}{\partial z_1} \int_{x_*-1}^{x+z_1} [\theta_0^1 + \theta_1^1(-s-1+x_*)] (1+i\lambda s) ds = 0 \\ z_1 = -x_* \end{aligned} \quad (V-24a)$$

$$\begin{aligned} (1+i\lambda x) [\theta_0^1 + \theta_1^1(-x-1+x_*)] - \frac{\partial}{\partial z} \int_{-1}^{x-z} (1-iks)(1+i\lambda s) ds \\ - \frac{\partial}{\partial z} \int_{x_*-1}^{x-z} [\theta_0^0 + \theta_1^0(-s-1+x_*)] (1+i\lambda s) ds = 0 \\ z = x_* \end{aligned} \quad (V-24b)$$

Product terms containing $(k\lambda) = \frac{k^2}{m}$ may be neglected as of higher order in k , yielding

$$(1+i\lambda x) [\theta_0^0 + \theta_1^0(-x-1+x_*)] + \frac{\partial e^{i\sigma}}{\partial z_1} \int_{-1}^{x+z_1} [1+i(\lambda+k)s] ds$$

$$+ \frac{\partial}{\partial z_1} \int_{x_*-1}^{x+z_1} \{ [\theta_0^1 + \theta_1^1(-s-1+x_*)] \}$$

$$+ i\lambda s [\theta_0^1 + \theta_1^1(-s-1+x_*)] \} ds = 0$$

$$z_1 = -x_* \quad (V-25a)$$

$$(1+i\lambda x) [\theta_0^1 + \theta_1^1(-x-1+x_*)] - \frac{\partial}{\partial z} \int_{-1}^{x-z} [1+i(\lambda+k)s] ds$$

$$- \frac{\partial}{\partial z} \int_{x_*-1}^{x-z} \{ [\theta_0^0 + \theta_1^0(-s-1+x_*)] + i\lambda s [\theta_1^0 + \theta_1^0(-s-1+x_*)] \} ds = 0$$

$$z = x_* \quad (V-25b)$$

Evaluating the indicated derivatives yields

$$(1+i\lambda x) [\theta_0^0 + \theta_1^0(-x-1+x_*)] + [1+i(k+\lambda)(x-x_*)] e^{i\sigma}$$

$$+ [\theta_0^1 + \theta_1^1(2x_*-x-1)] + i\lambda(x-x_*) [\theta_0^1 + \theta_1^1(2x_*-x-1)] \} = 0$$

$$(V-26a)$$

$$(1+i\lambda x) [\theta_0^1 + \theta_1^1 (-x-1+x_*)] + [1+i(\lambda+k)(x-x_*)]$$

$$+ \{ [\theta_0^0 + \theta_1^0 (2x_* - x - 1)] + i\lambda(x-x_*) [\theta_0^0 + \theta_1^0 (2x_* - x - 1)] \} = 0$$

(V-26b)

Thus:

$$\theta_0^0(1+i\lambda x) + \theta_1^0[(-x-1+x_*) + i\lambda x(-x-1+x_*)]$$

$$+ \theta_0^1[1 + i\lambda(x-x_*)] + \theta_1^1[(2x_* - x - 1) + i\lambda(x-x_*)(2x_* - x - 1)]$$

$$= -e^{i\sigma} [1 + i(k+\lambda)(x-x_*)] \quad (V-27a)$$

$$\theta_0^1[1 + i\lambda x] + \theta_1^1[(-x+1-x_*) + i\lambda x(-x+1-x_*)]$$

$$+ \theta_0^0[1+i\lambda x(x-x_*)] + \theta_1^0[(2x_* - x - 1) + i\lambda(x-x_*)(2x_* - x - 1)]$$

$$= -[1 + i(\lambda+k)(x-x_*)] \quad (V-27b)$$

This system may be solved at two points, x_1 and x_2 , for

θ_0^0 , θ_1^0 , θ_0^1 , and θ_1^1 .

2. Calculation Of The Potential

The potential is given by

$$\psi(x, y) = \Psi(x, z) e^{-i\lambda x} \quad (V-28)$$

where

$$\begin{aligned} \Psi(x, z) = & -\frac{1}{m} \int_{-1}^x [v^0(s) + u^0(s)] J_0[\omega \sqrt{(x-s)^2}] e^{i\lambda s} ds \\ & + \frac{1}{m} \int_{-1}^{x-x_*} [v^1(s) + u^1(s)] J_1[\omega \sqrt{(x-s)^2 - x_*^2}] e^{i\lambda s} ds. \end{aligned}$$

$$u^0(s) = u^1(s) = 0 \quad \text{for all } s \leq x_* - 1.$$

Thus

$$\begin{aligned} \Psi(x, z) = & -\frac{1}{m} \int_{-1}^x v^0(s) J_0[\omega \sqrt{(x-s)^2}] e^{i\lambda s} ds \\ & - \frac{1}{m} \int_{x_*-1}^x u^0(s) J_0[\omega \sqrt{(x-s)^2}] e^{i\lambda s} ds \\ & + \frac{1}{m} \int_{-1}^{x-x_*} v^1(s) J_0[\omega \sqrt{(x-s)^2 - x_*^2}] e^{i\lambda s} ds \\ & + \frac{1}{m} \int_{x_*-1}^{x-x_*} u^1(s) J_0[\omega \sqrt{(x-s)^2 - x_*^2}] e^{i\lambda s} ds \quad (V-29) \end{aligned}$$

Making the same small frequency approximations as in the previous section yields

$$\begin{aligned}
 \Psi(x, z) = & -\frac{1}{m} \int_{-1}^x v^0(s) (1+i\lambda s) ds \\
 & -\frac{1}{m} \int_{x_*-1}^x u^0(s) (1+i\lambda s) ds \\
 & + \frac{1}{m} \int_{-1}^{x-x_*} v^1(s) (1+i\lambda s) ds \\
 & + \frac{1}{m} \int_{x_*-1}^{x-x_*} u^1(s) (1+i\lambda s) ds \quad (V-30)
 \end{aligned}$$

From the general formulation

$$\Psi = \Phi^1 + \Phi^0 + \Psi^1 + \Psi^0 \quad (V-31)$$

Thus, along the reference blade

$$\begin{aligned}
 -m\Phi^0(x, z=0) &= \int_{-1}^x v^0(s) (1+i\lambda s) ds = \int_{-1}^x (1+iks) (1+i\lambda s) ds \\
 &= \int_{-1}^x [1+i(k+\lambda)s] ds = \left[s + i(k+\lambda) \frac{s^2}{2} \right]_{-1}^x \quad (V-32) \\
 &= x + i \frac{(k+\lambda)}{2} x^2 + 1 - i \left(\frac{k+\lambda}{2} \right)
 \end{aligned}$$

$$\phi^0(x, z=0) = -\frac{1}{m}[(1+x) + i(\frac{k+\lambda}{2})(x^2-1)] \quad (V-33)$$

By inspection

$$\phi^1(x, z_1=-x_*) = \frac{e^{i\sigma}}{m}\{(1+x-x_*) + i(\frac{k+\lambda}{2})[(x-x_*)^2-1]\} \quad (V-34)$$

$$-m\psi^0(x, z=0) = \int_{x_*-1}^x u^0(s)(1+i\lambda s)ds \quad (V-35)$$

$$= \int_{x_*-1}^x [\theta_0^0 + \theta_1^0(-s+x_*-1)](1+i\lambda s)ds$$

$$= \int_{x_*-1}^x \theta_0^0(1+i\lambda s) + \theta_1^0(-s+x_*-1)(1+i\lambda s)ds$$

$$= \theta_0^0[(x+1-x_*) + \frac{i\lambda}{2}(x^2-x_*^2+2x_*-1)]$$

$$+ \int_{x_*-1}^x \theta_1^0[-x+x_*-1+i\lambda(-s^2+sx_*-s)]ds$$

$$= \theta_0^0[(x+1-x_*) + \frac{i\lambda}{2}(x^2-x_*^2+2x_*-1)]$$

$$+ \theta_1^0\{(-\frac{s^2}{2}+sx_*-s)+i\lambda(-\frac{s^3}{3}+\frac{s^2x_*}{2}-\frac{s^2}{2})\} \Big|_{x_*-1}^x \quad (V-36)$$

$$\begin{aligned}
&= \theta_0^0 \left[(x+1-x_*) + \frac{i\lambda}{2} (x^2 - x_*^2 + 2x_* - 1) \right] \\
&+ \theta_1^0 \left\{ \left(-\frac{x^2}{2} + x_* - x \right) - \left[-\frac{(x_*-1)^2}{2} + x_* (x_* - 1) - (x_* - 1) \right] \right. \\
&+ i\lambda \left[\left(-\frac{x^3}{3} + \frac{x^2 x_*}{2} - \frac{x^2}{2} \right) + \frac{(x_*-1)^3}{3} - x_* \frac{(x_*-1)^2}{2} + \frac{(x_*-1)^2}{2} \right] \left. \right\}
\end{aligned}$$

$$\begin{aligned}
&= \theta_0^0 \left[(x+1-x_*) + \frac{i\lambda}{2} (x^2 - x_*^2 + 2x_* - 1) \right] \\
&+ \theta_1^0 \left\{ -\frac{x^2}{2} + x(x_* - 1) + \frac{(x_*-1)^2}{2} - (x_* - 1)^2 \right. \\
&+ i\lambda \left[-\frac{x^3}{3} + x^2 \frac{(x_*-1)}{2} + \frac{x_*^3}{3} - x_*^2 + x_* - \frac{1}{3} \right. \\
&\quad \left. \left. - \frac{x_*^3}{2} + x_*^2 - \frac{x_*}{2} + \frac{x_*^2}{2} - x_* + \frac{1}{2} \right] \right\}
\end{aligned}$$

$$\begin{aligned}
&= \theta_0^0 \left[(x+1-x_*) + \frac{i\lambda}{2} (x^2 - x_*^2 + 2x_* - 1) \right] \\
&+ \theta_1^0 \left\{ -\frac{x^2}{2} + x(x_* - 1) - \frac{(x_*-1)^2}{2} \right. \\
&+ i\lambda \left[-\frac{x^3}{3} + \frac{x^2 (x_*-1)}{2} - \frac{x_*^3}{6} + \frac{x_*^2}{2} - \frac{x_*}{2} + \frac{1}{6} \right] \left. \right\}
\end{aligned}$$

$$\begin{aligned}
\Psi^0 = & -\frac{1}{m}\{\theta_0^0[(x+1-x_*) + \frac{i\lambda}{2}(x^2 + x_*^2 + 2x_*-1)] \\
& + \theta_1^0\{-\frac{x^2}{2} + x(x_*-1) - \frac{(x_*-1)^2}{2} \\
& + i\lambda[-\frac{x^3}{3} + \frac{x^2(x_*-1)}{2} - \frac{(x_*-1)^3}{6}]\}\} \quad (V-37)
\end{aligned}$$

$m\psi^1(x, z_1=-x_*)$ may be evaluated by substituting $x-x_*$ for x in the expression for $m\psi^0$ and exchanging θ_0^1 and θ_1^1 for θ_0^0 and θ_1^0

$$\begin{aligned}
m\psi^1(x, z_1=-x_*) = & \theta_0^1\{[(x-x_*)+1-x_*] + \frac{i\lambda}{2}[(x-x_*)^2 - x_*^2 + 2x_* - 1]\} \\
& + \theta_1^1\{-\frac{(x-x_*)^2}{2} + (x-x_*)(x_*-1) - \frac{(x_*-1)^2}{2} \\
& + i\lambda[-\frac{(x-x_*)^3}{3} + \frac{x^2(x_*-1)}{2} - \frac{(x_*-1)^3}{6}]\} \quad (V-38)
\end{aligned}$$

$$\begin{aligned}
= & \theta_0^1(x+1-2x_*) + \frac{i\lambda}{2}[(x^2-2xx_*+x_*^2) - x_*^2 + 2x_* - 1]\} \\
& + \theta_1^1\{-\frac{(x^2-2xx_*+x_*^2)}{2} + (x - \frac{3}{2}x_* + \frac{1}{2})(x_*-1) \\
& + i\lambda[-\frac{x^3}{3} + x^2x_* - xx_*^2 + \frac{x_*^3}{3} + (x^2-2xx_*+x_*^2)\frac{(x_*-1)}{2} \\
& - \frac{(x_*-1)^3}{6}]\}
\end{aligned}$$

$$\begin{aligned}
&= \theta_0^1 \{ (x+1-2x_*) + \frac{i\lambda}{2} [x^2 - 2xx_* + 2x_* - 1] \\
&\quad + \theta_1^1 \{ -\frac{x^2}{2} + xx_* - \frac{x_*^2}{2} + x(x-1) + \frac{1}{2}(1-3x_*)(x_*-1) \\
&\quad + i\lambda [-\frac{x^3}{3} + x^2 \frac{(3x_*-1)}{2} + x(-\frac{x_*^2-2xx_*^2-1)}{2} \\
&\quad \quad + \frac{x_*^3}{3} + \frac{x_*^3}{2} - \frac{1}{2}] \}
\end{aligned}$$

$$\begin{aligned}
\psi^1(x, z_1 = -x_*) \\
&= \frac{1}{m} \{ \theta_0^1 \{ (x+1-2x_*) + \frac{i\lambda}{2} [x^2 - 2xx_* + 2x_* - 1] \\
&\quad + \theta_1^1 \{ [-\frac{x^2}{2} + x(2x_*-1) - xx_*^2 + 2x_* - \frac{1}{2}] \\
&\quad + i\lambda [-\frac{x^3}{3} + x^2 \frac{(3x_*-1)}{2} + x \frac{(-3x_*^2-1)}{2} + 5\frac{x_*^3}{6} - \frac{1}{2}] \} \}
\end{aligned}$$

(V-39)

A comparison of the results for the full program and the approximation is given below for $k = 0.01$, $w = 0.05$, $\sigma = \rho$, $n = 2$, yielding $\omega^2 \approx 6.1 \times 10^{-3}$, $\lambda \approx 0.083$

	Full program	Approx
$x = .1285$		
ϕ	-5.363, .327i	-5.379, .549i
ϕ_x	-8.634, .361i	-8.66, .379i
$x = .5643$		
ϕ	-9.754, .809i	-9.804, 1.000i
ϕ_x	-12.234, .692i	-12.272, .7608i
C_{ℓ_α}	+31.658, -3.1032i	C_{ℓ_α} 31.7019, -3.2165i

VI. RESULTS

The collocation method was used to solve the partial differential equation resulting from the Gorelov approximation of transonic potential flow in an unstaggered cascade. The system was solved using both the spanning functions proposed by Gorelov in [4], resulting in the equations (V-16); and the Legendre polynomials, resulting in equations (V-15) with f_j replaced by the Legendre polynomial, P_j . The resulting values of C_{ℓ_α} for $k = .1$, $\tau = 1$, $\sigma = 1$ and seven collocation points on each blade are presented in figures VI-2, VI-3, and VI-4.

Figure VI -1 presents a diagram which is useful in commenting on the other results. This shows the location of the collocation points and first three interference reflections as a function of w expressed as a percentage of that portion of the chord subject to reflection. The collocation points are equally spaced throughout this interval, 12.5% from the leading edge of the interference zone, 12.5% between each pair of points and 12.5% from the blade trailing edge. The independent variable, w , is plotted vertically so that the dependent variable, percent of chord subject to interference, may be more conveniently visualized along the blade. (The curves are not precisely linear, but are very nearly so in the range shown.)

Figure VI -2 shows the C_{ℓ_α} calculated with $k = 0.0$ in comparison with the results obtained from Ackeret theory.

Agreement is good where there is no reflection and the portion of the blade subject to interference is affected by a constant interference potential, $w \geq 0.11$. Throughout the rest of the curve the results calculated here oscillate above and below the theoretical values. This appears to be due to the discrete nature of the approximation used in the collocation method. Rarely is the fraction of the chord subject to interference reflection equal to the fraction of the collocation points which feel it. Where the collocation point fraction lags, as near $w = 0.6$, the collocation results are lower than those due to Ackeret theory. When the collocation point fraction leads, as it does for $w \leq .04$ and briefly for $w \approx .08$, the the collocation results are higher than those due to Ackeret theory. The fault appears to be an intrinsic feature of the small number of points sampled. This results in a set of coefficients similar to those which would be obtained from a generalized Fourier series based on the integration of the Taylor series expansion about each point. This obviously cannot be a good approximation when both the function and its derivative are discontinuous at the reflections.

Figures VI -3 and VI -4 show the results of using Legendre polynomials and Gorelov's functions as spanning functions. The results for both formulations are identical. Gorelov's results are presented for comparison. Agreement is good for $w > 0.05$ except for an anomalous point, marked A .

It is believed that this anomaly is due to the location of the first reflection just ahead of the last collocation point (cf. "A" on Figure VI -1). This will yield a very small contribution from the reflection potential to the linear system from which the collocation points are determined. The resulting system will have a large dynamic range and may be ill-conditioned.

The discrepancy between these results, and those in [3] for $w < 0.5$ is still unexplained, as is the outlying value for $w = 0.5$.

The discontinuities in the imaginary results are believed to be due primarily to the reflection/collocation interaction explained above.

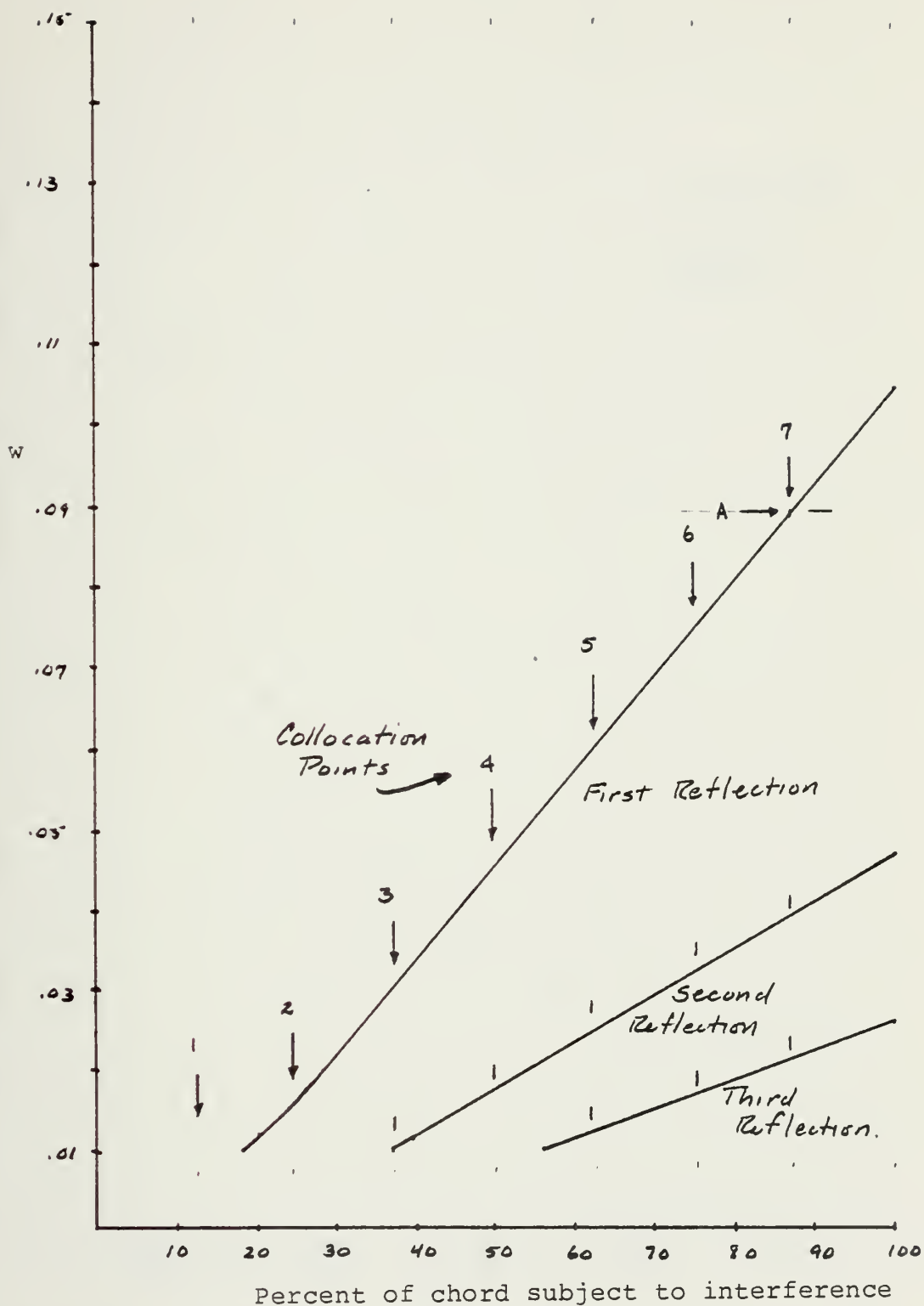


FIGURE VI-1. Location of Reflections and Collocation Points Shown as Percent of Chord Subject to Interference

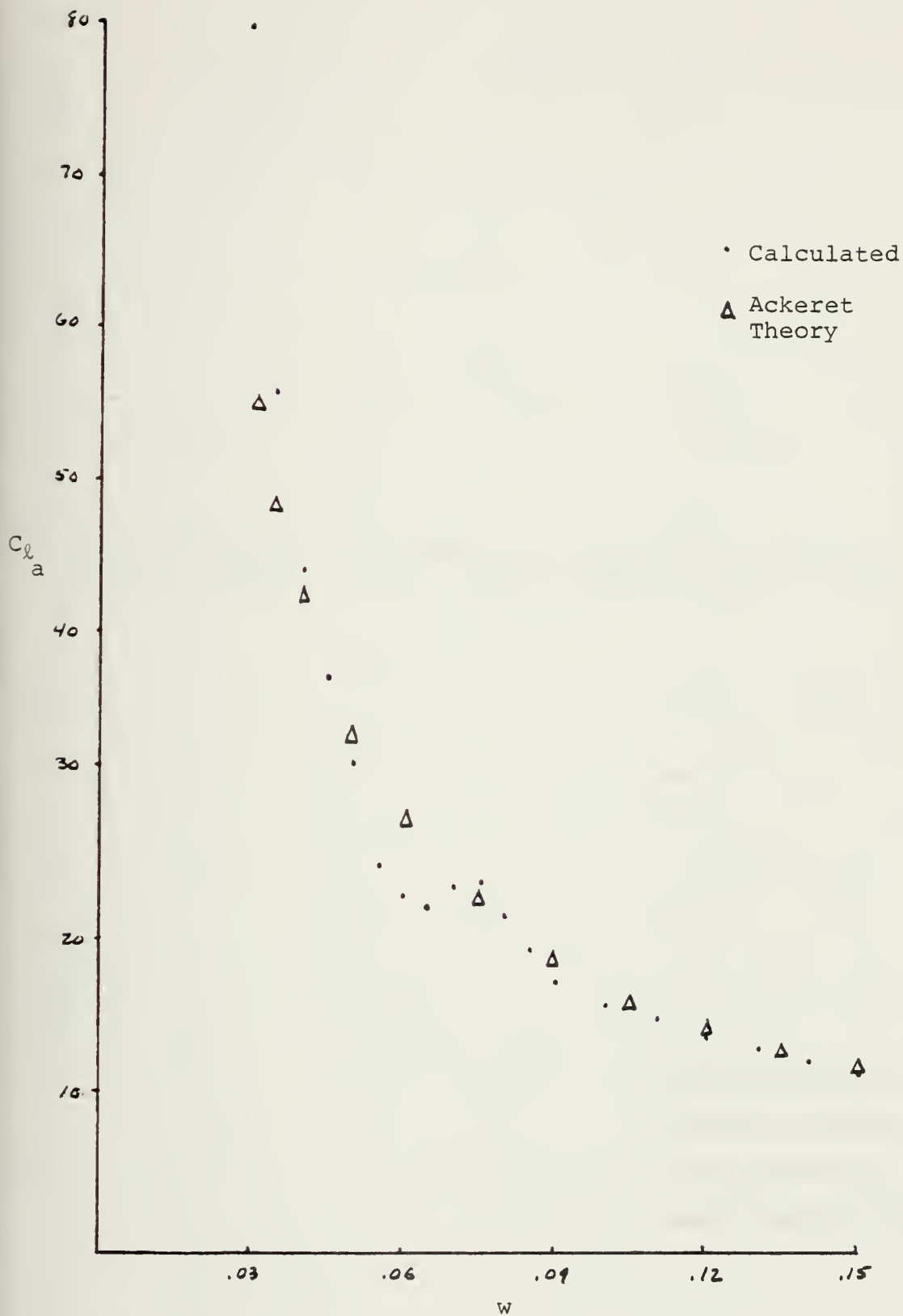


FIGURE VI-2. Comparison of Cl_α -vs- w to that Obtained from Ackeret Theory

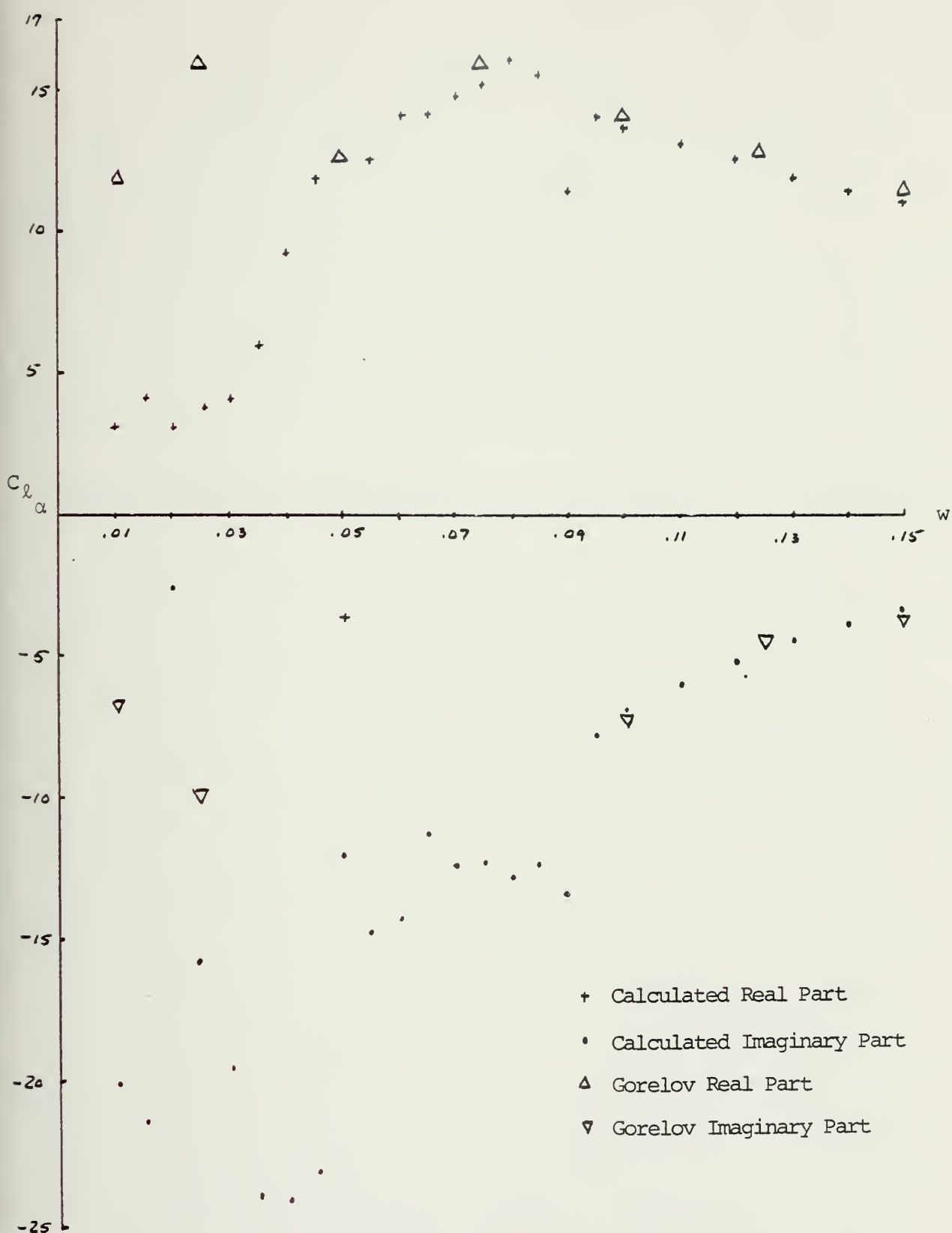


FIGURE VI-3. Plot of Cl_α -vs- w , Legendre Polynomials
 $k = 0.1$, $\tau = 1.0$, $\sigma = \pi$, $n = 7$
 compared with Gorelov's results

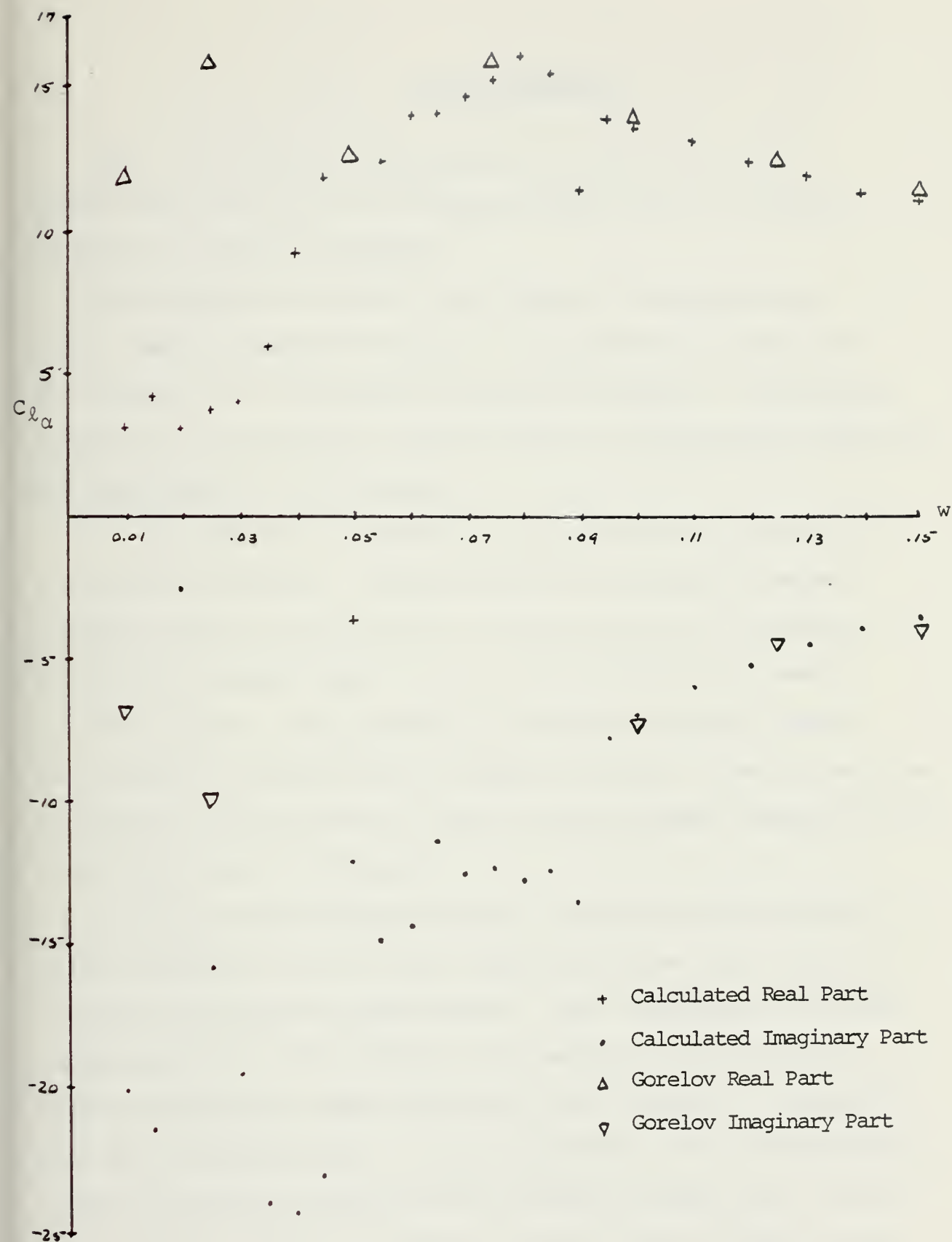


FIGURE VI-4. Plot of Cl_α -vs- w , Gorelov Spanning Function $k = 0.1$, $\tau = 1.0$, $\sigma = \pi$, $n = 7$ compared with Gorelov's results

VII . RECOMMENDATIONS

There are two recommendations to be made about the techniques used in the collocation method, and a new area in which it might be employed.

The program developed in the course of writing this thesis employs adaptive Simpson's integration to calculate the elements of a completely determined system. This system is solved to provide the coefficients of the spanning functions. Two improvements may be made:

1. The Simpson's integration scheme may be replaced by a Gaussian integrator. Experience has shown that several thousand function evaluations are required by the Simpson's integration routine when C_{λ_α} is to be evaluated for small w . This entails large amounts of computer time and leads to increased accumulations of numerical error. Use of Gaussian integration would probably improve both of these characteristics with little loss of accuracy.

2. The present program treats a completely determined system of dimension $2n+1$ by $2n+1$, and then solves that system to find the collocation coefficients. This procedure has worked satisfactorily in this thesis, but may not work as well at higher frequencies where the final linear system of equations may be ill-conditioned. As an alternative, it is recommended that the boundary conditions be applied at more than n points, say m points, where m is twice or three times as many points, and that the least squares technique be used to determine the

the collocation coefficients which give the minimum square error over-all. This may be thought of as "sampling more data" in order to get more information about the unknown function. The present program could be easily modified in this regard by replacing the spanning function matrix, Q1ZINT, by a new matrix of the form

$$Q1ZINT' = X^T X$$

where X is the new m by n+1 ($m > n+1$) matrix, and replacing the present right-hand-side vector, Q1COF with

$$Q1COF' = X^T Y$$

where Y is the new m by 1 right-hand-side vector. An alternative would be to employ a prepackaged statistical linear regression routine after either modifying the routine to accept complex data, or transforming the present system into a larger system of real numbers only.

The new area in which the collocation method might be employed is the calculation of the potential flow about a staggered cascade. The method could be employed to calculate both the potential in the channel and above the upper blade. The program presented has been designed to enable the

calculation of flow within the channel of a staggered cascade. Unfortunately, there was not enough time to extend the study to this case.

APPENDIX A
PROGRAM DESCRIPTION

This section describes the computer program used to calculate the interference solution to the Gorelov linearization for unsteady transonic flow in a channel. The program written in IBM Fortran IV with the basic structure outlined by Stevens [5]. The basic points are:

1. Organization of the program into small subroutines, each of which performs a specific task.
2. Transmission data to and from subroutines via a formal parameter argument list. No common statements are used.

The end objective is code which is both easy to modify and maintain.

Each subroutine is designed with optional diagnostic printing of its input and output. This is controlled by the parameter IPT. The diagnostic output is printed (only) if $IPT > 0$. Each routine accepts IPT, sets $IOT = IPT - 1$, and then passes IOT as the print parameter to routines it calls. By this method, diagnostic output can be "cascaded" to any desired level. Large initial values of IPT should be avoided because of the spectacular amount of output which can be generated by the double integrals within Q1DCOF.

1. Main Program; including subroutines READ and ABSA.

The basic structure is given in Figure A-1. MAIN calls READ to read input data and then ABSA to calculate the

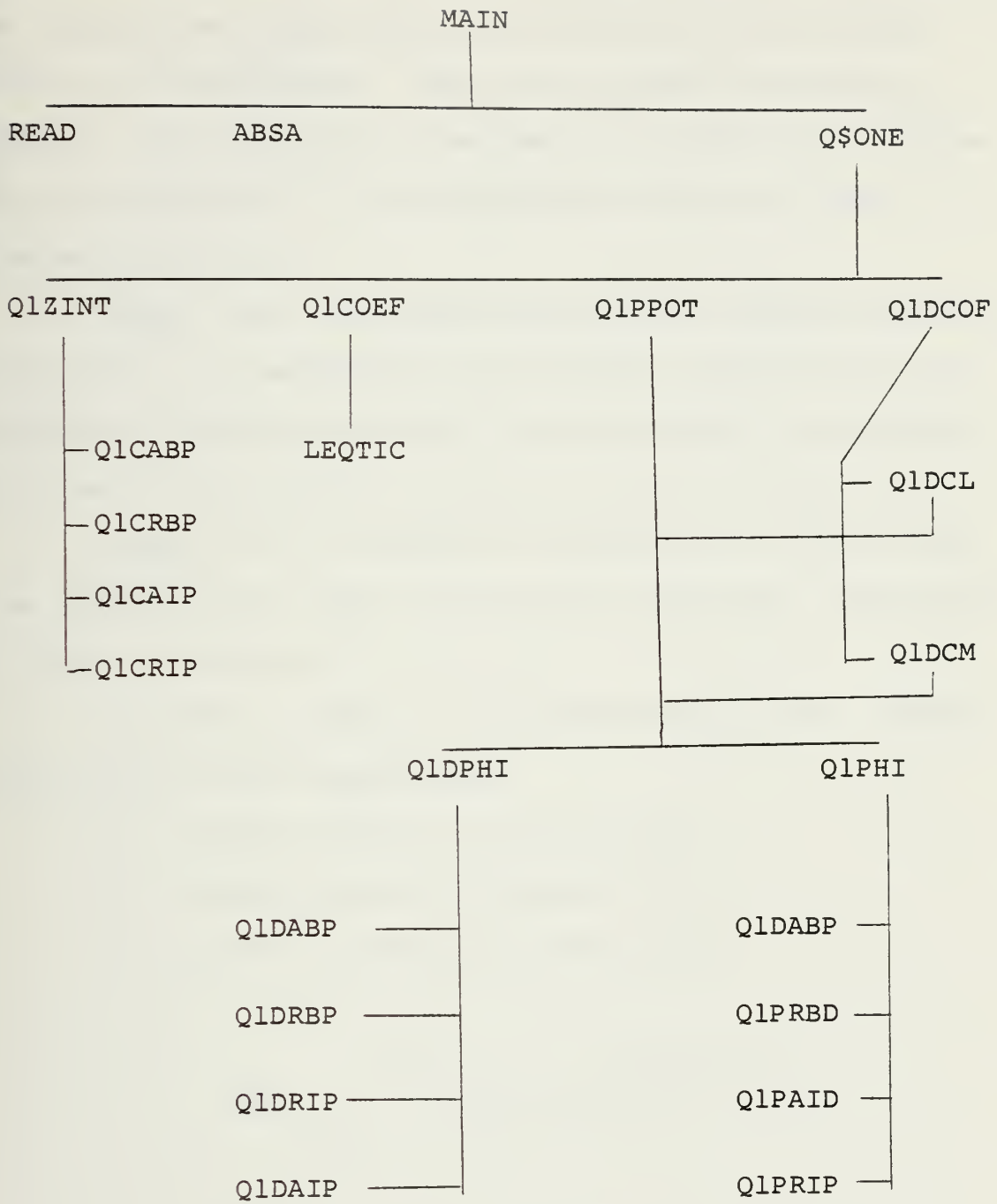


Figure A-1. Program Hierarchy

collocation points. The version of ABSA shown evenly spaces the collocation points across that portion of the blade subject to interference. ABSA may be easily replaced if different point spacing is desired, or if additional points are to be added for an overdetermined system and least squares approximation.

2. Q\$ONE This subroutine controls the actual potential calculation. It performs no calculation itself, but calls subordinate subroutines where the calculations are actually performed. The calling hierarchy is shown in Figure A-1.

3. Q1ZINT This subroutine calculates the linear equation system arising from the boundary conditions. Hierarchy is shown in Figure A-2.

The matrix output is carried through Q1INT. Q1ZINT calls the following subprograms

- a. Q1CRBP returns the value of ϕ_z^0
- b. Q1CABP returns the value of $\phi_{z_1}^1$
- c. Q1CRIP returns the values of ψ_z^0

$$\frac{\partial}{\partial z} \int_{-1+x_*}^{x-z} f_j(s) J_0[\omega \sqrt{(x-s)^2 - z^2}] ds$$

where f_i is one of the set of i elementary functions, $j=1,n$

- d. Q1CAIP returns the values of $\psi_{z_1}^1$

Q1ZINT

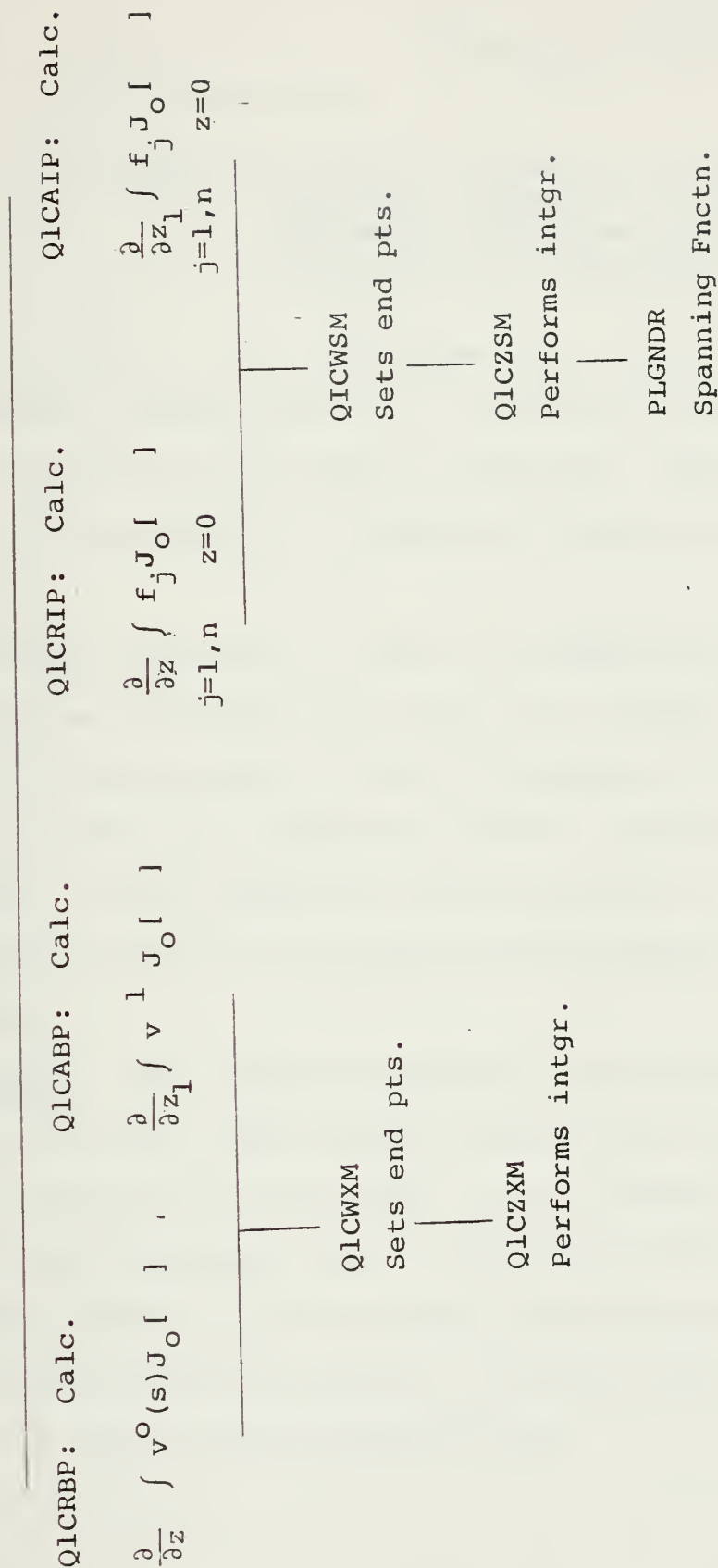


Figure A-2

$$\frac{\partial}{\partial z_1} \int_{-1+\text{OFFSET}+x_*}^{x+z_1} f_j(s) J_0[\omega \sqrt{(x-s)^2 - y_1^2}] ds$$

where f_j is one of the set of elementary functions. OFFSET is a parameter included to facilitate program conversion to a staggered cascade

e. PLGNDR is the subprogram which returns $f_j(x)$, the elementary spanning function. No other routine contains explicit reference to the spanning function. This facilitates easy replacement of the spanning functions should this be desired.

QlCRBP and QlCABP in turn call QlCWXM and QlCZXM. QlCWXM computes end-points and then calls QlCZXM, a complex integration routine based on SIMP by Shampine and Allen [6]. QlCAIP and QlCRIP call QlCWSM and QlCZSM to perform the integration. QlZINT passes the constant matrix to QlCOEF in the array QlINT and the right-hand-side vector in the array QlCOF.

4. QlCOEF This subroutine employs the IMSL routine LEQT1C to solve the linear system received from QlZINT. The resulting coefficients are QlABCF for the adjacent blade and QlRBCF for the reference blade. LEQT2C, the high precision complex IMSL routine may be directly substituted for LEQT1C. QlCOEF may be rewritten to employ the generalized inverse required for least squares approximation

$$A = (x^T x)^{-1} x^T y \quad \text{where } x = Q1INT$$

$$y = Q1COF$$

after first performing the multiplication necessary to replace Q1INT and Q1COF with the proper matrix products in the call to LEQT1C.

5. Q1PPOT This subroutine calculates the potential, ϕ , and ϕ_x , at each collocation point along the reference blade but only if Q1PPOT receives a value of IPT > 0, requiring IPT \geq 2 on input to the main program. If IPT \leq 0, then the subroutine is exited before any calculations are performed. This subroutine is most useful for debugging Q1ZINT and Q1COEF. Q1PPOT calls Q1PABP, Q1PRBP, Q1PRIP, Q1PAIP, Q1DABP, Q1DRBP, Q1DRIP, and Q1DAIP, all of which will be described in the next section.

6. Q1DCOF This subroutine calculates the dimensionless coefficients of lift and moment; C_{l_α} , C_{m_α} . Its internal hierarchy is shown in Figure A-3.

- a. Q1DCL calculates the nondimensional complex coefficient C_{l_α}
- b. Q1DCM calculates the nondimensional complex coefficient C_{m_α} .
- c. Q1PRBP and Q1PABP calculate the potentials due to the reference and adjacent blades respectively. Q1PWXM and Q1PZXM are called to perform the actual integration.

- d. Q1PRIP and Q1PAIP calculate the interference potentials along the reference and adjacent blades. Q1PZSM is called to perform the integration.
- e. Q1DRBP, Q1DABP, Q1DRIP, and Q1DAIP correspond exactly to subroutines above except that the value returned is the partial derivative of the potential with respect to X. Q1DWXM, Q1DZSM, and Q1DXSM perform the corresponding integrals.

6. Program Listing The program listing shown below incorporates the Legendre functions as spanning functions. Listings for a subroutine employing Gorelov's spanning function and the linear approximation program follow.


```

C      IMPLICIT REAL*8(A-T,G,P,R-Y), COMPLEX*16(Q,Z)
C      DIMENSION X(13), Q2PT(13), Q2CP(13)
C      BLCK ONE READ AND EDIT DATA
C      CALL ERRSET(208,256,-1,1)
C      WRITE(6,910)
C      CALL READ(CK,DR,CW,RHO,OFFSET,SIGMA,N,NF,IPT)
C      IF(IPT.GT.0)WRITE(6,950)DK,DR,DW,SIGMA,OFFSET,RHG,N,NF
C      S1C FCRMAT(,1,5X,'GCRRLCV CASCADE PROGRAM')
C      95C FCRMAT(,0,5X,'INFUT VALUES TRANSMITTED TO MAIN PROGRAM:',/,
C      1,10X,'DK',13X,'CR',13X,'DW',10X,'SIGMA',10X,'CFFSET',/,
C      1,10X,'OK',13X,'CR',13X,'DW',10X,'SIGMA',10X,'CFFSET',/,
C      1,10X,'5(E12.5,3X)',/,5X,'NFCN',
C      2,0,10X,'RHC',12X,'N',12,4X,I2)
C      3,/,10X,'1(E12.5,3X)',12,4X,I2)
C      CALL ABSA(N,OFFSET,X,RHO,CW)
C
C      BLCK TWO      CALLS CALCULATION ROUTINES FCR ZCNE ONE AND ZCNE TWO
C      CALL Q$CNE(CK,DR,CW,RHO,OFFSET,SIGMA,N,NF,IFT,X)
C      GC TC 1
C      END
C      SUBROUTINE READ (CK,DR,DW,RHO,OFFSET,SIGMA,N,NF,IPT)
C      IMPLICIT REAL*8(A-T,G,P,R-Y)
C      READ(5,505) DK,DR,CW,RHP,OFFSET,SIGMA,N,NF,IPT
C      IF (DK.LT.0.0D0) STOP
C      IF (IPT.GT.0) WRITE (6,510)
C      GAMMA = 1.4CO
C      CFC = RHP * [SQRT((GAMMA + 1.0D0) * DW)
C      RFC = DR
C      IF(N.LE.13) GO TC 1
C      N = 13
C      WRITE(6,935)
C      1 IF(OFFSET.LE.1.9DC) GO TO 2
C      WRITE(6,940)
C      OFFSET = CFFSET-1.0D0
C      GO TO 1
C      CONTINUE
C      IF (IPT.GT.0) WRITE (6,925) DK,DR,DW,SIGMA,CFFSET,RFC,N,NF,IPT
C      RETURN
C      905 FCRMAT (6F10.4,3I2)
C      910 FCRMAT (,1,10X,'STAGGERED SUPERSCHNIC CASCADE PROGRAM')
C      925 FCRMAT (,0,10X,'DK',13X,'DR',13X,'DW',10X,'SIGMA',10X,'OFFSET',
C      1,10X,'5(E12.5,3X)',/,5X,'NFCN',2X,'IPT',
C      2,0,10X,'RHC',12X,'N',12,4X,I2)
C      3,/,10X,'1(E12.5,3X)',12,4X,I2,4X,I2)
C      935 FCRMAT(,0,5X,'ORIGINAL N TOO LARGE (.GT.1.9) - RESET TO N = 13')
C      940 FCRMAT(,0,5X,'OFFSET TOO LARGE (.GT.1.9), RESET AS CFFSET =
C      1,OFFSET - 1.0D0)
C      ENDC

```


CLDRGC245
 QLDRGC255
 QLDRGC260
 QLDRGC265
 QLDRGC270
 QLDRGC275
 QLDRGC280
 QLDRGC285
 QLDRGC290
 QLDRGC295
 QLDRGC300
 QLDRGC305
 QLDRGC310
 QLDRGC315
 QLDRGC320
 QLDRGC325
 QLDRGC330
 QLDRGC335
 QLDRGC340
 QLDRGC345
 QLDRGC350
 QLDRGC355
 QLDRGC360
 QLDRGC365
 QLDRGC370
 QLDRGC375
 QLDRGC380
 QLDRGC385
 QLDRGC390
 QLDRGC395
 QLDRGC400
 QLDRGC405
 QLDRGC410
 QLDRGC415
 QLDRGC420
 QLDRGC425
 QLDRGC430
 QLDRGC435
 QLDRGC440
 QLDRGC445
 QLDRGC450
 QLDRGC455
 QLDRGC460
 QLDRGC465
 QLDRGC470
 QLDRGC475
 QLDRGC480

```

SUBROUTINE ABSA (N,OFFSET,X,DR,CW
)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX*16(Q,Z)
DIMENSION X(13)
XINT = (2.000-DR)/DFLOAT(N+1)
XL = DR - 1.000 + 1.000-8
CC 10 I = 1,N
X(I) = XL + (XINT*DFLOAT(I))
IF(X(I).EQ.0.000) X(I) = .1E-14
10 CONTINUE
RETURN
END
SUBROUTINE ($ONE(CK,CR,CW,RHO,OFFSET,SIGMA,N,NF,IPT,X)
IMPLICIT REAL*8(A-H,O,P,R-Y), COMPLEX*16(Z,C)
DIMENSION Q1COF(26), Q1INT(26,26), Q1RBP(13), Q1ABP(13)
DIMENSION Q1RBCF(13), Q1ABCF(13)
DIMENSION X(13)
IF(IPT.GT.0)WRITE(6,950)DK,CR,RHO,OFFSET,SIGMA,N,NF,IPT
ICT = IPT - 1
950 FORMAT(10 SUBROUTINE Q$ONE ENTERED WITH: ',/,
1. ',5X,'DK',13X,'RHO',12X,'OFFSET',9X,'SIGMA',10X,
2. ',5X,'NF',12X,'IPT',/,
3. ',5X,'I2',2X,'I3')
CALL Q1ZINT(DK,DR,DW,RHO,OFFSET,SIGMA,N,X,ICT,C1CCF,C1INT)
CALL Q1COEF(Q1COF,Q1INT,N,IOT,Q1AECF,Q1RBCF)
CALL Q1PPCT(DK,DR,CW,RHO,OFFSET,SIGMA,N,X,C1AECF,C1RBCF,ICT)
ICT = 0
CALL Q1CCCF(CK,DR,CW,RHO,OFFSET,SIGMA,N,Q1AECF,Q1RBCF,ICT)
RETURN
END
SUBROUTINE Q1ZINT(DK,DR,DW,RHO,OFFSET,SIGMA,N,X,
IPT,Q1COF,Q1INT)
IMPLICIT REAL*8(A-H,O,P,R-Y), COMPLEX*16(Z,Q)
DIMENSION Q1COF(26), Q1INT(26,26), Q1INTRP(13), Q1INTAP(13)
DIMENSION X(13)
990 1. ',10X,'Q1ZINT ENTERED WITH: ',/,
2. ',10X,'DK',13X,'RHO',12X,'OFFSET',9X,'SIGMA',10X,
3. ',10X,'IPT',/,
4. ',10X,'I2',2X,'I3')
CCCNST = CDEXP(DCMPLX(0.000,SIGMA))
IF (IPT.GT.0) WRITE (6,990) DK,DR,RHO,OFFSET,SIGMA,N,IPT
ICT = IPT - 1
GAMMA = 1.400
CLAMD = 1.000*(GAMMA+1.000)*CW
CC 90 I = 1,N
IN = I + N

```

CC

QLDR0485
QLDR0490
QLDR0495
QLDR0500
QLDR0505
QLDR0510
QLDR0515
QLDR0520
QLDR0525
QLDR0530
QLDR0535
QLDR0540
QLDR0545
QLDR0550
QLDR0555
QLDR0560
QLDR0565
QLDR0570
QLDR0575
QLDR0580
QLDR0585
QLDR0590
QLDR0595
QLDR0600
QLDR0605
QLDR0610
QLDR0615
QLDR0620
QLDR0625
QLDR0630
QLDR0635
QLDR0640
QLDR0645
QLDR0650
QLDR0655
QLDR0660
QLDR0665
QLDR0670
QLDR0675
QLDR0680
QLDR0685
QLDR0690
QLDR0695
QLDR0700
QLDR0705
QLDR0710
QLDR0715
QLDR0720

```

XSTN = X(I)
XD = XSTN - DR
CEXP = CDEXP(DCMPLX(0.0D0, DLAMCA*XSTN))
CALL Q1CABP(DK, DR, DW, RHO, OFFSET, SIGMA, XSTN, CINTAP, N, IOT)
CALL Q1CRIP(DK, DR, DW, RHO, OFFSET, XSTN, QINTRP, N, ICT)
DC 20 J = 1, N
JN = N + J
J1 = J - 1
Q1INT(I, J) = PLGNDP(XSTN, DR, J1) * CEXP
Q1INT(IN, J) = QINTRP(J)
Q1INT(I, JN) = QINTAP(J)
Q1INT(IN, JN) = PLGNDP(XSTN - OFFSET, CR, J1) * CEXP
CCONTINUE
2C Q1COF(IN) = -Q1CRBP(DK, DR, DW, RHO, XSTN, IOT)
Q1COF(I) = -Q1CABP(DK, DR, DW, RHO, OFFSET, SIGMA, XSTN, IOT)
90 CONTINUE
RETURN
END
CCOMPLEX FUNCTION Q1CRBP*16(DK, DR, DW, RHO, XSTN, IPT)
IMPLICIT REAL*8 (A-F, C, P, R-Y), COMPLEX*16 (Q, Z)
DIMENSION QINP(2)
IF (IPT.GT.0) WRITE(6,990) DK, DW, RHO, XSTN, IPT
IF (IPT.LE.0) THEN
  10X, 'Q1CRBP ENTERED WITH: ', /
  10X, 'DK, ', 11X, 'DR, ', 11X, 'DW, ', 11X, 'RHO, ', 10X, 'XSTN, ', 9X, 'IPT, '
  /
  20X, '10X, 5(E12.5, ', 11X, '13)
  IF (XSTN.LE.RHO-1.0D0) GOTO 20
  IF (XSTN.GT.2.0D0) GOTO 20
  ICT = IPT - 1
  QCK = DCMPLX(0.0D0, DK)
  CALL Q1CWXM(DK, DR, DW, RHO, XSTN, QINP, IOT)
  Q1CRBP = -QCK*QINP(2) - QINP(1)
  IF (IPT.LE.0) RETURN
  GOTO 30
20 Q1CRBP = DCMPLX(0.0D0, 0.0D0)
  IF (IPT.LE.0) RETURN
30 WRITE(6,995) Q1CRBP
995 FCORMAT('0, 10X, 'Q1CRBP = ', E14.7, ', ', E14.7)
RETURN
END
CCOMPLEX FUNCTION Q1CABP*16(DK, DR, DW, RHO, OFFSET, SIGMA, XSTN, IPT)
IMPLICIT REAL*8 (A-F, O, P, R-Y), COMPLEX*16 (C, Z)
DIMENSION QINP(2)
IF (IPT.GT.0) WRITE(6,990) DK, CR, DW, RHO, OFFSET, SIGMA, XSTN, IPT
IF (IPT.LE.0) THEN
  10X, 'Q1CABP ENTERED WITH: ', /
  10X, 'DK, ', 11X, 'CR, ', 11X, 'DW, ', 11X, 'RHO, ', 10X, 'OFFSET, ', 7X,
  10X, 'SIGMA, ', 8X, 'XSTN, ', 9X, 'IPT, ', /
  20X, '10X, 7(E12.5, ', 11X, '13)
  XSTN = XSTN - OFFSET
  IF (XSTN.LE.RHO-1.0D0) GOTO 20

```


QLDR0725
QLDR0730
QLDR0735
QLDR0740
QLDR0745
QLDR0750
QLDR0755
QLDR0760
QLDR0765
QLDR0770
QLDR0775
QLDR0780
QLDR0785
QLDR0790
QLDR0795
QLDR0800
QLDR0805
QLDR0810
QLDR0815
QLDR0820
QLDR0825
QLDR0830
QLDR0835
QLDR0840
QLDR0845
QLDR0850
QLDR0855
QLDR0860
QLDR0865
QLDR0870
QLDR0875
QLDR0880
QLDR0885
QLDR0890
QLDR0895
QLDR0900
QLDR0905
QLDR0910
QLDR0915
QLDR0920
QLDR0925
QLDR0930
QLDR0935
QLDR0940
QLDR0945
QLDR0950
QLDR0955
QLDR0960

```

IF(XASTN.GT.2.000) GOTO 20
ICT = IPT - 1
CCK = DCMPLX(0.000,DK)
QCONST = CDEXP(DCMPLX(0.000,SIGMA))
CALL QICWXM(DK,DR,DW,RHO,XASTN,CINF,IOT)
QICABP = -(CDK*QINP(2) + QINP(1)) * QCONST
IF(IPT.LE.0) RETURN
CC TO 30
2C QICABP = DCMPLX(0.000,0.000)
30 IF(IPT.LE.0) RETURN
555 WRITE(6,995) QICABP
FCRMT(0,10X,'QICABP = ',E14.7,' ',E14.7)
RETURN
END
SLROUTINE QICWXM(DK,DR,DW,RHO,XSTN,QINP,IPT)
N IS THE MAXIMUM DEGREE OF THE TERM U IN THE INTEGRALS
IMPLICIT REAL * 8 (A-H,Q,P,R-Y), COMPLEX * 16 (Z,Q)
DIMENSION QINP(2)
IF(IPT.GT.0) WRITE(6,990) DK,DR,RHC,XSTN,IPT
FORMAT(0,10X,'QICWXM ENTERED WITH ARGUMENTS:',/,
1,10X,DK,16X,CR,16X,RHC,15X,XSTN,14X,IPT,/,
2,10X,4(E13.6,5X),12,5X,I3)
ICT = IPT - 1
B = XSTN - RHO - 1.0D-10
A = -1.000
CALL QICZXM(DK,DR,CW,RHO,XSTN,A,B,1,QANS,IOT)
QINP(1) = QANS
CALL QICZXM(DK,DR,CW,RHO,XSTN,A,B,2,QANS,IOT)
QINP(2) = QANS
IF(IPT.LE.0) RETURN
WRITE(6,995)
FCRMT(0,10X,'J',16X,'QINP(1)',
1,10X,I = 1,2
DC 1001 I = 1,2
996 FORMAT(0,10X,I3,5X,E12.6,' ',E12.6)
1001 WRITE(6,996) I, QINP(I)
RETURN
END
SLROUTINE QICZXM(DK,DR,DW,RHC,XSTN,A,B,J,QANS,IPT)
IMPLICIT REAL * 8 (A-H,Q,P,R-Y), COMPLEX * 16 (F,G,Z)
DIMENSION FV(5),LORR(30),F1(30),F2(30),F3(30),
1 AREST(30),QUEST(30),EPST(30),QPSUM(30)
1 F(X) = (X**J1)*CDEXP(QEXP*(X))
2 * (OMEGA*RHO/(DSQRT((XSTN-X)*(XSTN-X)-YY),IER))
MMBSJ1(OMEGA*DSQRT((XSTN-X)*(XSTN-X)-YY),IER)
GAMMA = 1.40

```

C
C
C

QLDR0965
QLDR0970
QLDR0975
QLCR0980
QLDR0985
QLDR0990
QLDR0995
QLCR1000
QLCR1005
QLDR1010
QLDR1015
QLDR1020
QLDR1025
QLCR1030
QLDR1035
QLDR1040
QLDR1045
QLCR1050
QLCR1055
QLDR1060
QLDR1065
QLDR1070
QLCR1075
QLCR1080
QLDR1085
QLDR1090
QLDR1095
QLDR1100
QLDR1105
QLDR1110
QLDR1115
QLDR1120
QLDR1125
QLCR1130
QLDR1135
QLDR1140
QLDR1145
QLDR1150
QLDR1155
QLDR1160
QLDR1165
QLDR1170
QLCR1175
QLDR1180
QLDR1185
QLDR1190
QLDR1195
QLDR1200

```

DM2 = ( GAMMA + 1.000 ) * DW
CMEGA = DSQRT(DK*CK*(1.000-DM2)/(CM2*DM2))
YY = RHO * RHC
CLAMDA = DK/DM2
QEXP = DCMLPX(0.00C,CLAMDA)
J1 = J-1
ACC = 1.00-6
U = 9.00-13
IF (IPT.GT.C) WRITE(6,990)DK,DR,DH,RHO,XSTN,A,B,J,I,FT
FCRMAT(0.15X,'Q1CZM ENTERED WITH ARGUMENTS:',/,
1.15X,DK,13X,CR,13X,DW,10X,RHC,12X,XSTN,11X,
2.14X,8.14X,J,2X,IPT,/,
3.15X,7E14.7,/,12,2X,13)
EFCURU = 4.0*U
IFLAG = 1
EPS = ACC
GERROR = DCMLPX(0.000,0.000)
LVL = 1
LCRR(LVL) = 1
GPSUM(LVL) = 0.0
ALPHA = A
CA = B - A
AREA = 0.0
AREST = 0.0
FV(1) = F(ALPHA)
FV(3) = F(ALPHA + 0.5*DA)
FV(5) = F(ALPHA + DA)
KCUNT = 3
WT = DA/6.0
CEST = WT*(FV(1) + 4.0*FV(3) + FV(5))
CX = 0.5*DA
FV(2) = F(ALPHA + 0.5*DX)
FV(4) = F(ALPHA + 1.5*DX)
KCUNT = KCUNT + 2
WT = DX/6.0
CESTL = WT*(FV(1) + 4.0*FV(2) + FV(3))
QCESTR = WT*(FV(3) + 4.0*FV(4) + FV(5))
QCESTL = CESTL + CESTR
QCESTL = WT*(CDABS(FV(1)) + CDABS(4.0*FV(2)) + CDABS(FV(3)))
QCESTR = WT*(CDABS(FV(3)) + CDABS(4.0*FV(4)) + CDABS(FV(5)))
ARESTR = AREA + ((ARESTL + ARESTR) - AREST)
AREAL = CEST - QCESTL
QDIFF = QCESTR - QCESTL
IF(CDABS(QDIFF).LE.EPS*CDABS(AREA))GO TO 2
IF(CDABS(DX).LE.EFCURU*CDABS(ALPHA))GO TO 5
IF(LVL.GE.30)GO TO 5
IF(KCUNT.GE.2000)GO TO 6
LVL = LVL + 1
LCRR(LVL) = 0

```

1

QLDRI12105
 QLDRI12110
 QLDRI12115
 QLDRI12205
 QLDRI12210
 QLDRI12215
 QLDRI12305
 QLDRI12310
 QLDRI12315
 QLDRI12405
 QLDRI12410
 QLDRI12415
 QLDRI12505
 QLDRI12510
 QLDRI12515
 QLDRI12605
 QLDRI12610
 QLDRI12615
 QLDRI12705
 QLDRI12710
 QLDRI12715
 QLDRI12805
 QLDRI12810
 QLDRI12815
 QLDRI12905
 QLDRI12910
 QLDRI12915
 QLDRI13005
 QLDRI13010
 QLDRI13015
 QLDRI13105
 QLDRI13110
 QLDRI13115
 QLDRI13205
 QLDRI13210
 QLDRI13215
 QLDRI13305
 QLDRI13310
 QLDRI13315
 QLDRI13405
 QLDRI13410
 QLDRI13415
 QLDRI13505
 QLDRI13510
 QLDRI13515
 QLDRI13605
 QLDRI13610
 QLDRI13615
 QLDRI13705
 QLDRI13710
 QLDRI13715
 QLDRI13805
 QLDRI13810
 QLDRI13815
 QLDRI13905
 QLDRI13910
 QLDRI13915
 QLDRI14005
 QLDRI14010
 QLDRI14015
 QLDRI14105
 QLDRI14110
 QLDRI14115
 QLDRI14205
 QLDRI14210
 QLDRI14215
 QLDRI14305
 QLDRI14310
 QLDRI14315
 QLDRI14405

```

FIT(LVL) = FV(3)
F2T(LVL) = FV(4)
F3T(LVL) = FV(5)
DA = DX
DAT(LVL) = DX
AREST = ARESTL
ARESTT(LVL) = ARESTR
CEST = QESTL
CESTT(LVL) = QESTR
EPS = EPS/1.4
EPST(LVL) = EPS
FV(5) = FV(3)
FV(3) = FV(2)
GC TO 1
CERROR = QERROR + QDIFF/15.C
IF(LORR(LVL).EQ.C) GO TO 4
CSUM = QPSUM(LVL) + CSUM
LVL = LVL - 1
IF(LVL.GT.1) GO TO 3
QANS = CSUM - (B*J1) * CDEXP(QEXF*B)
IF(IPT.EQ.0) GO TO 11
IF(IFLAG.EQ.129) GO TO 11
IF(IFLAG.EQ.1) RETURN
WRITE(6,990) DK,DR,DW,RHO,XSTN,A,B,J,IPT
FCRMAT(,15X,RESULTS: QANS = ,E14.7,',,E14.7,/,
1,15X,IFLAG,2X,IER,5X,QERRCR,/,
2,15X,I3,2X,I3,5X,E14.7,.,,E14.7)
RETURN
QPSUM(LVL) = QSUM
LCRR(LVL) = 1
ALPHA = ALPHA + DA
DA = DAT(LVL)
FV(1) = F1T(LVL)
FV(3) = F2T(LVL)
FV(5) = F3T(LVL)
AREST = ARESTT(LVL)
QEST = QESTT(LVL)
EPS = EPST(LVL)
GC TO 1 2
IFLAG = 2 3
GC TO 2 3
GC TO 2 3
GC TO 2 3
END
SUBROUTINE CICAIP (CK,CR,DW,RFO,CFST,SGMA,XSTN,CCAIP,N,IPT)
IMPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX * 16 (C,Z)
  
```



```

DIMENSION CIMP(12), QCAIP(13)
IF (IPT.GT.0) WRITE(6,990) CK,DR,CW,RHO,OFST,SGMA,XSTN,IPT
FCRMA(0,10X,'Q1CAIP ENTERED WITH:',/,
1,10X,'CK',11X,'DR',11X,'Dh',11X,'RHC',1CX,'CFST',9X,'SGMA',9X
2,'XSTN',9X,'IPT',/,',,10X,7(E12.5,',,),I3)
XSTN=XSTN-OFST
IF(XSTN.LE.DR+RHO-1.0D0) GOTO 20
IF(XASTN.GT.2.0D0) GOTO 20
ICT=IPT-1
QCNST=CDEXP(CMPLX(0.0D0,SGMA))
CALL Q1CWSM(DK,DR,DW,RHO,XASTN,N,QINP,IOT)
DO 10 I=1,N
QCAIP(I)=CIMP(I)
CONTINUE
10 IF(IPT.LE.0) RETURN
GOTO 30
20 ZERC=DCMPLX(0.0C0,C.0D0)
DO 25 I=1,N
QCAIP(I)=ZERO
CONTINUE
25 IF(IPT.LE.0) RETURN
30 WRITE(6,995)
35 FCRMA(0,10X,'Q1CAIP RESULTS: J QCAIF(J)')
CC 40 J=1,N
WRITE(6,996) J,QCAIP(J)
356 FCRMA(0,26X,I2,3X,E14.7,',',E14.7)
40 CONTINUE
RETURN
ENL
SUBROUTINE Q1CRIP (CK,DR,DW,RHC,CFFSET,XSTN,CCRIP,N,IPT)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX * 16 (C,Z)
DIMENSION CCRIP(13)
IF (IPT.GT.0) WRITE(6,990) CK,DR,CW,RHO,XSTN,IPT
FCRMA(0,10X,'CK',11X,'DR',11X,'Dh',11X,'RHC',1CX,
1,10X,'XSTN',9X,'IPT',/,',,10X,5(E12.5,',,),I3)
2,'XSTN',9X,'IPT',/,',,10X,5(E12.5,',,),I3)
IF(XSTN.LE.DR+RHC+OFFSET-1.0D0) GOTO 20
IF(XSTN.GT.2.0D0) GOTO 20
ICT=IPT-1
CALL Q1CWSM(DK,DR,DW,RHO,XSTN,N,CCRIP,IGT)
IF(IPT.LE.0) RETURN
GOTO 30
20 ZERC=DCMPLX(0.0C0,C.0D0)
CC 25 I=1,N
CCRIP(I)=ZERO
35 IF(IPT.LE.0) RETURN
356 FCRMA(0,10X,'Q1CRIP RESULTS: J QCRIF(J)')
995

```

```

QLDR1445
QLCR1450
QLDR1455
QXQLCR1460
QLDR1465
QLDR1470
QLDR1475
QLDR1480
QLDR1485
QLDR1490
QLDR1495
QLDR1500
QLDR1505
QLDR1510
QLDR1515
QLDR1520
QLDR1525
QLDR1530
QLDR1535
QLDR1540
QLDR1545
QLDR1550
QLDR1555
QLDR1560
QLDR1565
QLDR1570
QLDR1575
QLDR1580
QLDR1585
QLDR1590
QLDR1595
QLDR1600
QLDR1605
QLDR1610
QLDR1615
QLDR1620
QLDR1625
QLDR1630
QLDR1635
QLDR1640
QLDR1645
QLDR1650
QLDR1655
QLDR1660
QLDR1665
QLDR1670
QLDR1675
QLDR1680

```



```

DC 40 J = 1,N
WRITE (6,556) J,QCRIP(J)
FCRMAP(1,26X,12,3X,E14.7,',',E14.7)
4C CCNTINUE
RETURN
ENC
SUBROUTINE C1CWSM (CK,DR,DW,RHO,XSTN,N,QINF,IPT)
N IS THE MAXIMUM DEGREE OF THE TERM U IN THE INTEGRALS
IMPLICIT REAL * 8 (A-H,O,P,R-Y), COMPLEX * 16 (Z,C)
DIMENSION QINP(13)
IF (IPT.GT.0) WRITE (6,590) DK,DR,FHC,XSTN,N,IPT
FCRMAP(1,10X,'Q1CWSM ENTERED WITH ARGUMENTS:',/,
1,10X,'DK',16X,'DR',16X,'RHO',15X,'XSTN',14X,'N',6X,'IPT',/,
2,10X,'4(E13.6,5X),12,5X,13)
IOT = IPT - 1
B = XSTN - RHO - 1.0D-10
A = DR - 1.0D0
DC 30 J = 1,N
CALL Q1CZSM(DK,DR,DW,RHO,XSTN,A,B,J,QANS,IOT)
QINF(J) = QANS
CCNTINUE
30 IF (IPT.LE.0) RETURN
WRITE (6,995)
FCRMAP(1,10X,'Q1CWSM RESULTS:',/,
1,11X,'J',6X,'QINP(1)',
DC 1001 I = 1,N
FCRMAP(1,10X,13,5X,E12.6,',',E12.6)
556 FORMAT(1,10X,13,5X,E12.6,',',E12.6)
1001 WRITE (6,996) I,QINP(I)
RETURN
END
SUBROUTINE Q1CZSM(DK,DR,DW,RHO,XSTN,A,B,J,QANS,IPT)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX*16 (F,Q,Z)
DIMENSION FV(5),LCRR(20),F1T(30),F2T(30),F3T(30),DAT(30),
1 ARESTT(30),QESTT(30),EPST(30),QPSUM(30)
1 F(X) = PLGNCR(X,DR,J1)*CDEXP(QEXP*(X))
1 * (CMEGA*RHO/(LSQRT((XSTN-X))*(XSTN-X)-YY))* (IER)
2 MBSJ1(OMEGA*DSQRT((XSTN-X)*(XSTN-X)-YY),IER)
GAMMA = 1.4D0
CM2 = (GAMMA + 1.0D0) * DW
CMEGA = CSQRT(DK*CK*(1.0D0-DM2)/(CM2*CM2))
YY = RHC * RHO
CLAMDA = DK/DM2
QEXP = DCMPLX(0.0D0,[LAMDA])
J1 = J-1
ACC = 1.0D-6
U = 9.0D-13

```

C
C
C

QLCRI1685
QLCRI1690
QLCRI1695
QLCRI1700
QLCRI1705
QLCRI1710
QLCRI1715
QLCRI1720
QLCRI1725
QLCRI1730
QLCRI1735
QLCRI1740
QLCRI1745
QLCRI1750
QLCRI1755
QLCRI1760
QLCRI1765
QLCRI1770
QLCRI1775
QLCRI1780
QLCRI1785
QLCRI1790
QLCRI1795
QLCRI1800
QLCRI1805
QLCRI1810
QLCRI1815
QLCRI1820
QLCRI1825
QLCRI1830
QLCRI1835
QLCRI1840
QLCRI1845
QLCRI1850
QLCRI1855
QLCRI1860
QLCRI1865
QLCRI1870
QLCRI1875
QLCRI1880
QLCRI1885
QLCRI1890
QLCRI1895
QLCRI1900
QLCRI1905
QLCRI1910
QLCRI1915
QLCRI1920


```

950 IF (IFT.GT.0) WRITE(6,990)DK,DR,CW,RHO,XSTN,A,E,J,IPT
FCRMAT(0,15X,'Q1CZSM ENTERED WITH ARGUMENTS:',/,
1,15X,'DK',13X,'CR',13X,'CW',10X,'RHO',12X,'XSTN',11X,
2,A,14X,'B',14X,'J',2X,'IPT',/,
3,15X,'7(E14.7',,},12,2X,13),
EFCURU = 4.C*U
IFLAG = 1
EPS = ACC
CERROR = DCMLPX(0.000,0.000)
LVL = 1
LCRR(LVL) = 1
CFSUM(LVL) = 0.0
ALPHA = A
DA = B - A
AREA = C.0
AREST = 0.0
FV(1) = F(ALPHA)
FV(3) = F(ALPHA) + 0.5*DA
FV(5) = F(ALPHA + DA)
KCUNT = 3
WT = DA/6.0
QUEST = WT*(FV(1) + 4.0*FV(3) + FV(5))
DX = 0.5*DA
FV(2) = F(ALPHA + 0.5*DX)
FV(4) = F(ALPHA + 1.5*DX)
KCUNT = KCUNT + 2
WT = DX/6.0
QUESTL = WT*(FV(1) + 4.0*FV(2) + FV(3))
QUESTR = WT*(FV(3) + 4.0*FV(4) + FV(5))
QSUM = QUESTL + QUESTR
ARESTL = WT*(CDABS(FV(1)) + CDAES(4.0*FV(2))) + CDABS(FV(3)))
ARESTR = WT*(CDABS(FV(3)) + CDABS(4.0*FV(4)) + CDABS(FV(5)))
AREA = ARESTL + ARESTR
GDIFF = AREST - QSUM
IF(CDABS(GDIFF).LE.EPS*CDABS(AREA))GO TO 2
IF(DABS(CX).LE.EFOURU*CDABS(ALPHA))GO TO 5
IF(LVL.GE.3)GO TO 5
IF(KCUNT.GE.200)GC TC 6
LVL = LVL + 1
LCRR(LVL) = 0
F1T(LVL) = FV(3)
F2T(LVL) = FV(4)
F3T(LVL) = FV(5)
DAT(LVL) = DX
DATEST(LVL) = CX
ARESTL = ARESTR
ARESTT(LVL) = ARESTR
QUEST = QUESTL

```

QLCR1920
 QLCR1930
 QLCR1935
 QLCR1940
 QLCR1945
 QLCR1950
 QLCR1955
 QLCR1960
 QLCR1965
 QLCR1970
 QLCR1975
 QLCR1980
 QLCR1985
 QLCR1990
 QLCR1995
 QLCR2000
 QLCR2005
 QLCR2010
 QLCR2015
 QLCR2020
 QLCR2025
 QLCR2030
 QLCR2035
 QLCR2040
 QLCR2045
 QLCR2050
 QLCR2055
 QLCR2060
 QLCR2065
 QLCR2070
 QLCR2075
 QLCR2080
 QLCR2085
 QLCR2090
 QLCR2100
 QLCR2105
 QLCR2110
 QLCR2115
 QLCR2120
 QLCR2125
 QLCR2130
 QLCR2135
 QLCR2140
 QLCR2145
 QLCR2150
 QLCR2155
 QLCR2160


```

CESTT(LVL) = QESTR
EPS = EPS/1.4
FV(5) = FV(3)
FV(3) = FV(2)
GO TO 1
QERROR = QERROR + CDIFF/15.0
IF(LCRR(LVL).EQ.0) GO TO 4
QSUM = QPSUM(LVL) + QSUM
IF(LVL.GT.1) GO TO 3
CANS = FLGNCR(B,CR,J1) * CDEXP(QEXP*B) - QSUM
IF(IPT.GT.C) GO TO 11
IF(IER.EQ.1) RETURN
WRITE(6,990) DK,DR,DW,RHC,XSTN,A,E,J,IPT
995 WRITE(6,995) CANS,IFLAG,IER,QERR,CF
FCRMAT(, , ,15X, ,RESULTS: QANS = E14.7, , ,E14.7, /,
1, ,15X, ,IFLAG, ,2X, ,IER, ,5X, ,CEFFCF, /,
2, ,15X,13,2X,13,5X,E14.7, , ,E14.7)
RETURN
QPSUM(LVL) = QSUM
LCRR(LVL) = 1
ALPHA = ALPHA + DA
DA = DAT(LVL)
FV(1) = FIT(LVL)
FV(3) = F2T(LVL)
FV(5) = F3T(LVL)
AREST = ARESTT(LVL)
CEPS = QESTT(LVL)
GC TO 1 2
IFLAG = 2
GC TO 2 3
IFLAG = 2
GC TO 2
END
REAL FUNCTION PLGNDR*(X,CR,N)
IMPLICIT REAL*8(A-F,O-Z)
IF(N.EQ.0) GOTO 10C
X2 = X*X
GC TO (101,103,104,105,106,107,108,109,110,111,112), N
100 PLGNCR = 1.000
101 RETURN = X
102 PLGNDR = ((3.00C)*X2-1.00C)/2.000
RETURN

```



```

103 PLGNDR = ((5.000*X2 - 3.000)*X/2.000
RETURN
104 PLGNDR = ((3.501*X2 - 3.001)*X2 + 3.000)/8.000
RETURN
105 PLGNDR = ((6.301*X2 - 7.001) *X2 +1.501)*X/8.000
RETURN
106 PLGNDR=((231.000*X2-315.000)*X2+105.000)*X2-5.000)/16.000
RETURN
107 PLGNDR=((429.000*X2-693.000)*X2+315.000)*X2-35.000)
1 *X/16.000
RETURN
108 PLGNDR=((6435.000*X2-1202.000)*X2+6930.000)*X2
1 -1260.000)*X2+35.000)/128.000
RETURN
109 PLGNDR=((12155.000*X2-25740.000)*X2+18018.000)
1 *X2-4620.000)*X2+315.000)/128.000
RETURN
110 PLGNDR=((146185.000*X2-109395.000)*X2+50000.000)
1 *X2-30030.000)*X2-3465.000)*X2-63.000)/256.000
RETURN
111 PLGNDR=((188175.000*X2-230945.000)*X2+218750.000)*X2
1 -90090.000)*X2+15015.000)*X2-693.000)*X2/256.000
RETURN
112 PLGNDR=((1676039.000*X2-19395535.000)*X2+2078505)*X2
1 -1021020.000)*X2+225225.000)*X2-18018.000)*X2-231.000)/1024.000
RETURN
END
SUBROUTINE C1COEF( Q1COF,Q1INT,N,IPT,Q1ABCF,Q1RBCF)
IMPLICIT REAL * 8(A-H,O,P,R-Y), COMPLEX * 16 (Z,C)
DIMENSION Q1COF(26), Q1INT(26,26), ZHA(300)
DIMENSION C1ABCF(13),Q1RBCF(13)
IF (IPT.GE.C) WRITE (6,90)
IE = 26
N2 = 1
N2 = 2*N
IF (IPT.LE.0) GO TO 5
WRITE (6,98) N,N2
FCRMAT(3,5X,Q1COF ENTERED WITH ',I2,' DEG PWR SERIES (',I2,
58 1, ' SQUARE MATRIX'),)
DC 2 I = 1,N2
WRITE(6,92) I, I, Q1COF(I)
FCFMAT(10,10X,Q1COF EQUATION SYSTEM, ROW ',I2,/,
92 1, ',10X,Q1COF(',I2,') = ', E14.7, ',E14.7),
DC 2 J = 1,N
J2=J+N
WRITE(6,91) I,J,Q1INT(I,J),I,J2,C1INT(I,J2)
91 1,15X,2('QINT(',I2, ', ',I2,') = ',E14.7, ',E14.7,10X))
2 CONTINUE

```

Q1DR2405
 Q1DR2410
 Q1DR2415
 Q1DR2420
 Q1DR2425
 Q1DR2430
 Q1DR2435
 Q1DR2440
 Q1DR2445
 Q1DR2450
 Q1DR2455
 Q1DR2460
 Q1DR2465
 Q1DR2470
 Q1DR2475
 Q1DR2480
 Q1DR2485
 Q1DR2490
 Q1DR2495
 Q1DR2500
 Q1DR2505
 Q1DR2510
 Q1DR2515
 Q1DR2520
 Q1DR2525
 Q1DR2530
 Q1DR2535
 Q1DR2540
 Q1DR2545
 Q1DR2550
 Q1DR2555
 Q1DR2560
 Q1DR2565
 Q1DR2570
 Q1DR2575
 Q1DR2580
 Q1DR2585
 Q1DR2590
 Q1DR2595
 Q1DR2600
 Q1DR2605
 Q1DR2610
 Q1DR2615
 Q1DR2620
 Q1DR2625
 Q1DR2630
 Q1DR2635
 Q1DR2640


```

5  IA = 26
   IJCB=0
   CALL LECTIC(QLINT,N2,IA,QICCF,M,IE,IJOB,ZWA,IER)
   IF(IER.EQ.0) GOTO 30
   IF(IER.EQ.129) GO TO 10
   WRITE(6,93)
93  FORMAT('0',10X,'QICCEF - ITERATIVE IMPROVEMENT FAILED, MATRIX TOO
      1 ILL-CONDITIONED. USE RESULTS WITH CAUTION.')
   GO TO 30
10  WRITE(6,95)
10  FORMAT('0',10X,'QICCEF - MATRIX ALGORITHMICALLY SINGULAR. CCEFFIC
      1 IENTS SET TO ZERO.')
   ZERO = DCMLPX(0.0DC,(.000)
   DO 20 I = 1,N
   I2 = I+N
   QICOF(I) = ZERO
   QICOF(I2) = ZERO
   CCNTINUE
   CCNTINUE = 1,N
   DO 35 I = 1+N
   IABCF(I) = QICOF(IN)
   QIRBCF(I) = QICOF(I)
   CCNTINUE
   IF(IPT.LE.0) RETURN (6,94)
   IF(IPT.GE.0) WRITE (6,94)
   DO 40 I = 1,N
   I1 = I-1
   WRITE(6,99) I, I1, QIRBCF(I), QIABCF(I)
   CCNTINUE
   DO 55 I = 1,N
   FCFMAT('0',5X,I2,10X,2(E14.7,5X,E14.7,10X))
   FCFMAT('0',10X,'SUBROUTINE QICCEF - COMPLEX POWER SERIES COEFFIC
      1 IENTS')
   FCFMAT('0',5X,'INDEX',7X,'DEG FCLY',4X,'REFERENCE BLADE TERMS QIC
      3 CCF(INDEX)',7X,'ADJACENT BLADE TERMS QICOF(2*INDEX),')
   RETURN
   ENDC
   FUNCTION IQIFC(I)
   .....
   IQIFC IS A FUNCTION SUBROUTINE DESIGNED TO PRCDUCE FACTRIALS
   .....
   IF(I.EQ.0) GO TO 11
   IF(I.EQ.1) GO TO 11
   IQIFC=I
   I1=I-1
   DO 10 J=1,I1
   IQIFC=IQIFC*(I-J)
10

```

QLDR2645
 QLDR2650
 QLDR2655
 QLDR2660
 QLDR2665
 QLDR2670
 QLDR2675
 QLDR2680
 QLDR2685
 QLDR2690
 QLDR2695
 QLDR2700
 QLDR2705
 QLDR2710
 QLDR2715
 QLDR2720
 QLDR2725
 QLDR2730
 QLDR2735
 QLDR2740
 QLDR2745
 QLDR2750
 QLDR2755
 QLDR2760
 QLDR2765
 QLDR2770
 QLDR2775
 QLDR2780
 QLDR2785
 QLDR2790
 QLDR2795
 QLDR2800
 QLDR2805
 QLDR2810
 QLDR2815
 QLDR2820
 QLDR2825
 QLDR2830
 QLDR2835
 QLDR2840
 QLDR2845
 QLDR2850
 QLDR2855
 QLDR2860
 QLDR2865
 QLDR2870
 QLDR2875
 QLDR2880

C
 C
 C


```

QDRIPP = QLDRIIP(DK,DR,DW,RHO,OFFSET,XSTN,CIRBCF,N,IOT)
QCAIPO = QIDAIP(DK,DR,DW,RZERO,OFFSET,SIGMA,XSTN,QIABCF,N,IOT)
QDAIPP = QDAIP(DK,DR,DW,RHO,OFFSET,SIGMA,XSTN,QIABCF,N,IOT)
QCR = QDRO + QDAF + QCRIPPO + QCAIPP
QDA = QDRP + QDAO + QCRIPP + QDAIFC
QCPHI(I)=QICPHI(DK,DR,DW,RHO,OFFSET,SIGMA,N,CIABCF,CIRBCF,
1 XSTN,IOT)
WRITE(6,95) I,XSTN
WRITE(6,91) QCR,QCRO,QDAP,QDRIPO,CDAIPP
WRITE(6,92) CCA,QCRP,QDAO,QCRIPP,CDAIPO
QCRRI(I) = QCR
QCAA(I) = CDA
95 FCRMAT('O X-STATIC NUMBER',I2,'XSTN =',F6.4,/,
1 BL TCTAL D(POT)/DX',14X,'REF EL D(POT)/CX',8X,
2 'ADJ BL D(PCT)/DX',8X,'REF EL INT D(POT)/DX',5X,
3 'ADJ BL INT D(POT)/DX')
10 CONTINUE
WRITE(6,994)
994 FCRMAT('O',1,10X,'SUMMARY LISTING',/,
1 'O',10X,'XSTN',7X,'SINGLE BLADE TOTAL POTENTIAL',6X,
1 'REF BLADE POTENTIAL',15X,'ADJ BLADE POTENTIAL',)
1 DC 20 I = 1,N
XSTN = X(I)
WRITE(6,94) XSTN,CPhi(I),QRR(I),QAA(I)
94 FCRMAT('O',1,10X,F6.4,3(5X,E14.7,/,E14.7))
20 CONTINUE
956 FCRMAT('O',1,10X,'XSTN',7X,'SINGLE ELADE TOTAL D(PCT)/DX',6X,
1 'REF ELADE D(POT)/DX',15X,'ADJ ELADE D(POT)/DX')
1 DC 50 I = 1,N
XSTN = X(I)
WRITE(6,94) XSTN,CPhi(I),QDRR(I),CDA(I)
50 CONTINUE
RETURN
END
SLBRCUTINE QIDCOF(CK,CR,DW,RHC,CFFSET,SIGMA,N,QIABCF,QIRBCF,IPT)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX*16 (Q,Z)
DIMENSION QIABCF(13), QIRBCF(13)
IF(IPT.GT.0)WRITE(6,990) DK,DR,CK,RHO,OFFSET,SIGMA,N,IPT
990 FCFMAT('O',1,10X,'QIDCOF - CALCULATION OF COMPLEX DIMENSI CNLESS AERG
1 DYNAMIC COEFFICIENTS',/,
3 'O',10X,'CK',13X,'DR',13X,'DW',12X,'RHO',12X,'OFFSET',5X,'SIGMA',
4 'O',10X,'N',3X,'IPT',/,
56(E12.5,3X),12,2X,I3)
1 IPT = IPT - 3
995 QICCL = QICCL(DK,DR,DW,RHO,OFFSET,SIGMA,N,QIABCF,CIRBCF,IOT)
QCCM = QIDCCM(DK,DR,DW,RHC,OFFSET,SIGMA,N,QIABCF,QIRBCF,IOT)
GAMMA = 1.4CO

```



```

TAL = (2.000*DSQRT((GAMMA + 1.000)*DW))/DR
WRITE (6,90) DK,TAU,DW,N,SIGMA,CCCL,CCCM
FCRMT(0.0,5X,DK = ,F6.3,,TAU = ,F7.4,,DW = ,F6.3,,N =
1      F12,,SIGMA = ,F6.3,,CL = ,F9.4,,F9.4,,CM = ,
2      F9.4,,F9.4)
RETURN
END
CCOMPLEX FUNCTION QIDCL*16(DK,DR,DW,RHO,OFFSET,SIGMA,N,QIABCF,CIRBCF,
1  IF,IPT) IT REAL*8(A - E,G,H,Q,F,R - Y), COMPLEX*16(F,Q,Z)
1  IMPLICATION QIABCF(13),QIRBCF(13)
C DIMENSION FV(5),FIT(60),FET(60),QEST(60),CPSUM(60)
C DIMENSION DAT(60),AREST(60),EPST(60)
C DIMENSION LCRR(60)
F(X) = (C1DFI(DK,DR,CW,RHO,OFFSET,SIGMA,N,C1ABCF,CIRBCF,X,ICT)
1  -GALPHA*CLPHI(CK,DR,CW,RHO,OFFSET,SIGMA,N,C1ABCF,CIRBCF,X,ICT))
0  IF (IPT.GT.C) WRITE (6,990) DK,CR,DW,RHO,CFFSET,SIGMA,N,IPT
FCRMT(0.0,10X,CLCL,ENTERED WITH: ,/
3  , ,10X,DK,13X,DR,13X,CK,13X,RHO,12X,OFFSET,9X,SIGMA,
4  6(E12.5,3X),12,2X,13)
5  A = -1.000
ECT = 1.000
1  ICT = IPT - 1
GAMMA = 1.400
CLAMDA = CK/((GAMMA + 1.000) * DW)
QALPHA = DCMLPX(0.000,CLAMDA-DK)
U = 9.0E-13
ACC = 1.00D-5
EFCURU = 4.0*U
IFLAG = 1
EFS = ACC
QERROR = DCMLPX(0.000,0.000)
LVL = 1
LCRR(LVL) = 1
QPSUM(LVL) = 0.0
ALPHA = A
DA = B - A
AREA = 0.0
AREST = 0.0
FV(1) = F(ALPHA)
FV(3) = F(ALPHA) + 0.5*DA
FV(5) = F(ALPHA) + DA
KCLNT = 3
WT = DA/6.0
CEST = WT*(FV(1) + 4.0*FV(3) + FV(5))
DX = 0.5*DA
F(2) = F(ALPHA) + 0.5*DX

```

Q1DR3365
 Q1DR3370
 Q1DR3375
 Q1DR3380
 Q1DR3385
 Q1DR3390
 Q1DR3395
 Q1DR3400
 Q1DR3405
 Q1DR3410
 Q1DR3415
 Q1DR3420
 Q1DR3425
 Q1DR3430
 Q1DR3435
 Q1DR3440
 Q1DR3445
 Q1DR3450
 Q1DR3455
 Q1DR3460
 Q1DR3465
 Q1DR3470
 Q1DR3475
 Q1DR3480
 Q1DR3485
 Q1DR3490
 Q1DR3495
 Q1DR3500
 Q1DR3505
 Q1DR3510
 Q1DR3515
 Q1DR3520
 Q1DR3525
 Q1DR3530
 Q1DR3535
 Q1DR3540
 Q1DR3545
 Q1DR3550
 Q1DR3555
 Q1DR3560
 Q1DR3565
 Q1DR3570
 Q1DR3575
 Q1DR3580
 Q1DR3585
 Q1DR3590
 Q1DR3595
 Q1DR3600

4


```

1
KCINT = 3
WT = DA/6.0
CEST = WT*(FV(1) + 4.0*FV(3) + FV(5))
DX = 0.5*DA
FV(2) = F(ALPHA + (.5*DX))
FV(4) = F(ALPHA + 1.5*DX)
KOUNT = KCINT + 2
WT = DX/6.0
CESTL = WT*(FV(1) + 4.0*FV(2) + FV(3))
CESTR = WT*(FV(3) + 4.0*FV(4) + FV(5))
CSUM = CESTL + CESTR
ARESTL = WT*(CDABS(FV(1)) + CDAES(4.0*FV(2)) + CDABS(FV(3)))
ARESTR = WT*(CDABS(FV(3)) + CDAES(4.0*FV(4)) + CDABS(FV(5)))
AREA = AREAL + ((ARESTL + ARESTR) - AREST)
COIFF = CEST - CSUM
IF(CDABS(COIFF).LE.EPS*DABS(AREA))GO TO 2
IF(CDABS(DX).LE.EFCURU*DABS(ALPHA))GO TO 5
IF(LVL.GE.60)GO TO 5
IF(KOUNT.GE.4000)GC TO 6
LVL = LVL + 1
LCRR(LVL) = 0
F1T(LVL) = FV(3)
F2T(LVL) = FV(4)
F3T(LVL) = FV(5)
DATA = DX
DAT(LVL) = [X
ARESTL = ARESTL
ARESTT(LVL) = ARESTR
CESTT(LVL) = CESTL
CESTT(LVL) = QESTR
EPS = EPS/1.4
EFST(LVL) = EPS
FV(5) = FV(3)
FV(3) = FV(2)
GC TO 1
QERRCR = CERROR + QCIF/15.0
IF(CLORR(LVL).EQ.0)GO TO 4
CSUM = QPSUM(LVL) + QSUM
LVL = LVL - 1
IF(LVL.GT.1)GO TO 3
IF(DCM = CSUM * 2.0C0
Q1DCM = CSUM * 2.0C0
IF(IPT.GT.0)GO TO 11
IF(IFLAG.EQ.1) RETURN
WRITE(6,990) DK,DRM,IFLAG,QERRCR,RHO,OFFSET,SIGMA,N,IPT
WRITE(6,995) Q1DCM,ULTS:Q1CCM = ,E14.7,,',E14.7,,',
FCRMT(, ,15X,IFLAG,2X,QERROR,,',
1, ,15X,I3,2X,E14.7,,',E14.7)
2, ,15X,I3,2X,E14.7,,',E14.7)
11
995

```

QLDR4085
 QLDR4090
 QLDR4095
 QLDR4100
 QLDR4105
 QLDR4110
 QLDR4115
 QLDR4120
 QLDR4125
 QLDR4130
 QLDR4135
 QLDR4140
 QLDR4145
 QLDR4150
 QLDR4155
 QLDR4160
 QLDR4165
 QLDR4170
 QLDR4175
 QLDR4180
 QLDR4185
 QLDR4190
 QLDR4195
 QLDR4200
 QLDR4205
 QLDR4210
 QLDR4215
 QLDR4220
 QLDR4225
 QLDR4230
 QLDR4235
 QLDR4240
 QLDR4245
 QLDR4250
 QLDR4255
 QLDR4260
 QLDR4265
 QLDR4270
 QLDR4275
 QLDR4280
 QLDR4285
 QLDR4290
 QLDR4295
 QLDR4300
 QLDR4305
 QLDR4310
 QLDR4315
 QLDR4320

QLCR4565
QLCR4570
QLDR4575
QLDR4580
QLDR4585
QLDR4590
QLDR4595
QLDR4600
QLDR4605
QLDR4610
QLDR4615
QLDR4620
QLDR4625
QLDR4630
QLDR4635
QLDR4640
QLDR4645
QLDR4650
QLDR4655
QLDR4660
QLDR4665
QLDR4670
QLDR4675
QLDR4680
QLDR4685
QLDR4690
QLDR4695
QLDR4700
QLDR4705
QLDR4710
QLDR4715
QLDR4720
QLDR4725
QLDR4730
QLDR4735
QLDR4740
QLDR4745
QLDR4750
QLDR4755
QLDR4760
QLDR4765
QLDR4770
QLDR4775
QLDR4780
QLDR4785
QLDR4790
QLDR4795
QLDR4800

```

IF(IPT.LE.0) RETURN
CCTC 60 = CCMPLX(C.C00,0.000)
20 QIPRBP = CCMPLX(C.C00,0.000)
IF(IPT.LE.0) RETURN
60 WRITE(6,995) QIPRBP
995 FORMAT('0',10X,'QIPRBP = ',E14.7,' ',E14.7)
RETURN
END
COMPLEX FUNCTION QIPABP*16(DK,CR,CW,RHO,OFFSET,SIGMA,XSTN,IPT)
IMPLICIT REAL*8 (A-F,C,P,R-Y), COMPLEX*16 (Q,Z)
DIMENSION QINP(2)
IF(IPT.GT.0) WRITE(6,990) DK,DR,DW,RHO,OFFSET,SIGMA,XSTN,IPT
990 FCRMAT('C',10X,'QIPABP ENTERED WITH:',/,
1 ' ',10X,'C',11X,'DR',11X,'DW',11X,'RHO',10X,'CFFSET',7X,
2 ' ',SIGMA,8X,'XSTN',9X,'IPT',/, ' ',10X,7(E12.5,','),I3)
XSTN = XSTN - OFFSET
IF(XSTN.LE.RHO-1.000) GOTO 20
ICT = IPT - 1
CCK = CCMPLX(0.000,DK)
QCONST = CDEXP(CCMPLX(0.000,SIGMA))
CALL QIPWXM(DK,DR,CW,RHC,XSTN,CINP,IOT)
QIPABP = (QCK*QINF(2) + QINP(1)) * QCONST
IF(IPT.LE.0) RETURN
CCTC 60
20 QIPABP = CCMPLX(C.CDC,0.000)
IF(IPT.LE.0) RETURN
60 WRITE(6,995) QIPABP
995 FCRMAT('0',10X,'QIPABP = ',E14.7,' ',E14.7)
RETURN
END
SUBROUTINE QIPWXM(CK,DR,DW,RHO,XSTN,CINP,IPT)
N IS THE MAXIMUM DEGREE OF THE TERM U IN THE INTEGRALS
IMPLICIT REAL*8 (A-F,C,P,R-Y), COMPLEX*16 (Z,Q)
DIMENSION QINP(2)
IF(IPT.GT.0) WRITE(6,990) DK,DR,RHC,XSTN,IPT
990 FCRMAT('C',10X,'QIPWXM ENTERED WITH ARGUMENTS:',/,
1 ' ',10X,'C',16X,'DR',16X,'RHO',15X,'XSTN',14X,'IPT',/,
2 ' ',10X,4(E13.6,5X),I2,5X,I3)
IOT = IPT - 1
B = XSTN - RHO - 1.00-10
A = -1.000
CALL QIPZXM(CK,DR,CW,RHO,XSTN,A,E,1,QANS,IOT)
QINP(1) = QANS
CALL QIPZXM(CK,DR,CW,RHC,XSTN,A,E,2,QANS,IOT)
QINP(2) = QANS
IF(IPT.LE.0) RETURN

```

CC

Q1DR5045
 Q1DR5050
 Q1DR5055
 Q1DR5060
 Q1DR5065
 Q1DR5070
 Q1DR5075
 Q1DR5080
 Q1DR5085
 Q1DR5090
 Q1DR5095
 Q1DR5100
 Q1DR5105
 Q1DR5110
 Q1DR5115
 Q1DR5120
 Q1DR5125
 Q1DR5130
 Q1DR5135
 Q1DR5140
 Q1DR5145
 Q1DR5150
 Q1DR5155
 Q1DR5160
 Q1DR5165
 Q1DR5170
 Q1DR5175
 Q1DR5180
 Q1DR5185
 Q1DR5190
 Q1DR5195
 Q1DR5200
 Q1DR5205
 Q1DR5210
 Q1DR5215
 Q1DR5220
 Q1DR5225
 Q1DR5230
 Q1DR5235
 Q1DR5240
 Q1DR5245
 Q1DR5250
 Q1DR5255
 Q1DR5260
 Q1DR5265
 Q1DR5270
 Q1DR5280

```

FV(2) = F(ALPHA + 0.5*DX)
FV(4) = F(ALPHA + 1.5*DX)
KCUNT = KCUNT + 2
WT = DX/6.0
QESTL = WT*(FV(1) + 4.0*FV(2) + FV(3))
QESTR = WT*(FV(3) + 4.0*FV(4) + FV(5))
QSUM = CESTL + QESTR
ARESTL = WT*(CDABS(FV(1)) + CDAES(4.0*FV(2)) + CDABS(FV(3)))
ARESTR = WT*(CDABS(FV(3)) + CDABS(4.0*FV(4)) + CCABS(FV(5)))
AREA = AREA + ((ARESTL + ARESTR) - AREST)
CDIFF = QEST - QSUM
CDIFF(CX) = LE.EPS*CDABS(AREA) GO TO 2
IF(DABS(CX).LE.EFOUR*CDABS(ALPHA)) GO TO 5
IF(LVL.GE.60) GO TO 5
IF(KOUNT.GE.2000) GC TC 6
LVL = LVL + 1
LCRR(LVL) = 0
F1T(LVL) = FV(3)
F2T(LVL) = FV(4)
F3T(LVL) = FV(5)
DA = DX
DAT(LVL) = CX
ARESTL = ARESTL
ARESTR = ARESTR
QESTL = QESTL
QESTR = QESTR
EPS = EPS/1.4
FV(5) = FV(3)
FV(3) = FV(2)
GC TO 1
QERROR = QERROR + CDIFF/15.0
IF(LORR(LVL).EQ.0) GC TC 4
QSUM = CPSUM(LVL) + QSUM
LVL = LVL - 1
IF(LVL.GT.1) GO TO 3
QANS = QSUM * Q2EXP / DM
IF(IPT.GT.0) GO TO 11
IF(IFLAG.EC.1) RETURN
WRITE(6,995) QANS,IFLAG,IER,QERR,A,E,J,IPT
FCRMT(1,15X,IFLAG,2X,IER,5X,QERR,A,E,J,IPT,E14.7,/,
1. ,15X,I3,I3,5X,E14.7,/,E14.7)
2. ,15X,I3,I3,5X,E14.7,/,E14.7)
RETURN
QFSUM(LVL) = QSUM
LCRR(LVL) = 1
ALPHA = ALPHA + DA
  
```

2 3

11 995

4

[illegible]


```

55C FCRMAT('0',10X,'Q1CRBP ENTERED WITH:','/,
1      ',10X,DK',11X,CR',11X,DW',11X,RHO',1C),XSTN',9X,'IPT',
2      ',/,10X,5(E12.5,',13)
      IF(XSTN.LE.RHO-1.0C0) GOTO 20
      ICT = IPT - 1
      QDK = DCPLX(0.0D0,DK)
      CALL Q1DWXM(DK,DR,DW,RHO,XSTN,QINP,IOT)
      Q1DRBP = -QDK*QINP(2) - QINP(1)
      IF(IPT.LE.0) RETURN
      GOTO 60
20 Q1DRBP = DCPLX(0.0D0,0.0C0)
      IF(IPT.LE.0) RETURN
      WRITE(6,995) Q1DREP
995 FCRMAT('0',10X,'Q1CRBP = ',E14.7,',',E14.7)
      RETURN
      ENDC
      COMPLEX FUNCTION Q1DABP*16(DK,DR,DW,RHO,CFFSET,SIGMA,XSTN,IPT)
      IMPLICIT REAL*8 (A-F,O,P,R-Y), CCMPLX*16(Q,Z)
      DIMENSION QINP(2)
      IF(IPT.GT.0) WRITE(6,990) DK,CR,CW,RHO,OFFSET,SIGMA,XSTN,IPT
990 FCRMAT('0',10X,DK',11X,CR',11X,DW',11X,CW',11X,RHO',10X,OFFSET',7X,
1      ',SIGMA',8X,XSTN',5X,IPT',/,',10X,7(E12.5,',13)
2      XSTN = XSTN - OFFSET
      IF(XSTN.LE.RHO-1.0C0) GOTO 20
      ICT = IPT - 1
      QDK = DCPLX(0.0D0,DK)
      CCONST = CDEXP(CCMPLX(0.0D0,SIGMA))
      CALL Q1DWXM(DK,DR,DW,RHO,XSTN,QINP,IOT)
      Q1DABP = (QDK*QINP(2) + QINP(1))*QCONST
      IF(IPT.LE.0) RETURN
      GOTO 60
20 Q1DABP = DCPLX(0.0D0,0.0C0)
      IF(IPT.LE.0) RETURN
      WRITE(6,995) Q1DAEP
995 FCRMAT('0',10X,'C1DABP = ',E14.7,',',E14.7)
      RETURN
      SUBROUTINE Q1DWXM(CK,DR,DW,RHO,XSTN,QINP,IPT)
      N IS THE MAXIMUM DEGREE OF THE TERM U IN THE INTEGRALS
      IMPLICIT REAL*8 (A-F,C,P,R-Y), CCMPLX*16(Z,C)
      DIMENSION QINP(2)
      IF(IPT.GT.0) WRITE(6,990) DK,CR,RFC,XSTN,IPT
990 FCRMAT('0',10X,Q1DWXM ENTERED WITH ARGUMENTS:','/,
1      ',10X,DK',16X,CR',16X,RHO',15X,XSTN',14X,IPT',/,
2      ',10X,4(E13.6,5X),12,5X,13)

```

Q1DR6245
 Q1DR6250
 Q1DR6255
 Q1DR6260
 Q1DR6265
 Q1DR6270
 Q1DR6275
 Q1DR6280
 Q1DR6285
 Q1DR6290
 Q1DR6295
 Q1DR6300
 Q1DR6305
 Q1DR6310
 Q1DR6315
 Q1DR6320
 Q1DR6325
 Q1DR6330
 Q1DR6335
 Q1DR6340
 Q1DR6345
 Q1DR6350
 Q1DR6355
 Q1DR6360
 Q1DR6365
 Q1DR6370
 Q1DR6375
 Q1DR6380
 Q1DR6385
 Q1DR6390
 Q1DR6395
 Q1DR6400
 Q1DR6405
 Q1DR6410
 Q1DR6415
 Q1DR6420
 Q1DR6425
 Q1DR6430
 Q1DR6435
 Q1DR6440
 Q1DR6445
 Q1DR6450
 Q1DR6455
 Q1DR6460
 Q1DR6465
 Q1DR6470
 Q1DR6475
 Q1DR6480

QLDR6485
 QLDR6490
 QLDR6495
 QLDR6500
 QLDR6505
 QLDR6510
 QLDR6515
 QLDR6520
 QLDR6525
 QLDR6530
 QLDR6535
 QLDR6540
 QLDR6545
 QLDR6550
 QLDR6555
 QLDR6560
 QLDR6565
 QLDR6570
 QLDR6575
 QLDR6580
 QLDR6585
 QLDR6590
 QLDR6595
 QLDR6600
 QLDR6605
 QLDR6610
 QLDR6615
 QLDR6620
 QLDR6625
 QLDR6630
 QLDR6635
 QLDR6640
 QLDR6645
 QLDR6650
 QLDR6655
 QLDR6660
 QLDR6665
 QLDR6670
 QLDR6675
 QLDR6680
 QLDR6685
 QLDR6690
 QLDR6695
 QLDR6700
 QLDR6705
 QLDR6710
 QLDR6715
 QLDR6720

```

ICT = IPT - 1
B = XSTN - RHO - 1.0D-10
A = -1.0D0
CALL Q1DZXM(CK, DR, DW, RHO, XSTN, A, E, 1, QANS, IOT)
QINP(1) = CANS
CALL Q1CZXM(CK, DR, CW, RHC, XSTN, A, E, 2, QANS, IOT)
CINP(2) = QANS
IF (IPT.LE.0) RETURN
WRITE(6,995)
1 FCRRAT(, , 1CX, , C1DWXM RESULTS: , / ,
, , 11X, , J, 6X, , QINP(1) , )
DC 1001 I = 1, 2
FCRRAT(, , 10X, I3, 5X, E12.6, , , E12.6)
1001 WRITE(6,996) I, CINP(I)
RETURN
END
SUBROUTINE Q1DZXM (DK, DR, DW, RHO, XSTN, A, B, J, CANS, IFT)
IMPLICIT REAL*8(A - E, G, H, M, O, P, R - Y), COMPLEX*16(F, G, Z)
DIMENSION FV(5), LCRR(60), F1(60), F2(60), F3(60), DAT(60),
1 AREST(60), QUEST(60), EPST(60), QPSUM(60)
1 F(X) = (X**J1)*CDEXP(QEXP*(X))
1 * MMESJ1((OMEGA * DSQRT((XSTN-X)*(XSTN-X) - YY)), IER)
2 GAMMA = 1.4C0
YY = RHO * RHO
CM2 = (GAMMA + 1.0C0) * DW
OMEGA = DSQRT (DK*DK*(1.0D0-DM2) / (CM2*DM2))
DLAMDA = DK/DM2
DM = DSQRT(CM2)
QEXP = CDEXP (DCMPLX (0.0C0, -CLAMDA*XSTN))
QEXP = CCMPLX(0.0D0, DLAMDA)
J1 = J - 1
U = 9.0D-13
ACC = 1.0D-6
IF (IPT.GT.0) WRITE(6,990)DK,DR,DW,RHO,XSTN,A,B,J,IFT
FCRRAT(, , 15X, , Q1DZXM ENTERED WITH ARGUMENTS: , / ,
1 , , 15X, , DK, , 13X, , ER, , 13X, , CW
2 , , 14X, , B, , 14X, , J, 2X, , IPT, , / ,
3 , , 15X, , 7(E14.7, , , 12, 2X, I3)
EFCURU = 4.C*U
IFLAG = 1
EPS = ACC
QERRR = DCMPLX(C.CDC,0.0D0)
LVL = 1
LCRR(LVL) = 1
QFSUM(LVL) = 0.0
ALPHA = A
DA = B - A
  
```


LR6725
 QLR6730
 QLR6735
 QLR6740
 QLR6745
 QLR6750
 QLR6755
 QLR6760
 QLR6765
 QLR6770
 QLR6775
 QLR6780
 QLR6785
 QLR6790
 QLR6795
 QLR6800
 QLR6805
 QLR6810
 QLR6815
 QLR6820
 QLR6825
 QLR6830
 QLR6835
 QLR6840
 QLR6845
 QLR6850
 QLR6855
 QLR6860
 QLR6865
 QLR6870
 QLR6875
 QLR6880
 QLR6885
 QLR6890
 QLR6895
 QLR6900
 QLR6905
 QLR6910
 QLR6915
 QLR6920
 QLR6925
 QLR6930
 QLR6935
 QLR6940
 QLR6945
 QLR6950
 QLR6955
 QLR6960

```

AFEA = 0.0
AREST = 0.0
FV(1) = F(ALPHA)
FV(3) = F(ALPHA + 0.5*CA)
FV(5) = F(ALPHA + CA)
KOUNT = 3
WT = DA/6.0
QEST = WT*(FV(1) + 4.0*FV(3) + FV(5))
DX = 0.5*DA
FV(2) = F(ALPHA + 0.5*DX)
FV(4) = F(ALPHA + 1.5*DX)
KOUNT = KOUNT + 2
WT = DX/6.0
GESTL = WT*(FV(1) + 4.0*FV(2) + FV(3))
GESTR = WT*(FV(3) + 4.0*FV(4) + FV(5))
CSLM = GESTL + GESTR
ARESTL = WT*(CDABS(FV(1)) + CDABS(4.0*FV(2)) + CCABS(FV(3)))
ARESTR = WT*(CDABS(FV(3)) + CDABS(4.0*FV(4)) + CDABS(FV(5)))
AFEA = AREST + (ARESTL + ARESTR)
QDIFF = QEST - QSUM
IF(CDABS(QDIFF).LE.EPS*DABS(AREA))GO TO 2
IF(DABS(DX).LE.EFCURU*DABS(ALPHA))GO TO 3
IF(LVL.GE.6)GO TC 5
IF(KOUNT.GE.400)GO TC 6
LVL = LVL + 1
LCRR(LVL) = 0
FIT(LVL) = FV(3)
FET(LVL) = FV(4)
FAT(LVL) = FV(5)
CA = DX
LAT(LVL) = CX
ARESTL = ARESTL
ARESTR = ARESTR
GESTL = ARESTR
GESTR = QEST
QEST = EPS/1.4
EPS = EPS
FV(3) = FV(2)
FV(5) = FV(3)
FV(2) = FV(1)
GO TO 1
GCRRCR = QERROR + QDIFF/15.0
IF(CLCRR(LVL).EQ.0)GO TO 4
QSUM = QPSUM(LVL) + QSUM
LVL = LVL - 1
IF(LVL.GT.1)GO TO 3
CANS = ((B*J1)*CCEXP(QEXP*B) - CSLM)*Q2EXP/DM
IF(IPT.GT.0)GO TC 11
IF(IFLAG.EQ.1) RETURN
  
```

1

2 3


```

11 WRITE(6,990) DK,DF,DW,RHO,XSTN,A,B,J,IPT
995 WRITE(6,995) QANS,IFLAG,IER,CERRCR
FORMAT(1,15X,'C1DZXM RESULTS: QANS = ',E14.7,' ',E14.7,' /',
1,15X,'IFLAG',2X,'IER',5X,'QERRCR',/,
2,15X,'13,2X,13,5X,E14.7',,E14.7)
RETURN
4 CFSUM(LVL) = QSUM
LCRR(LVL) = 1
ALPHA = ALPHA + CA
CA = DAT(LVL)
FV(1) = F1T(LVL)
FV(3) = F2T(LVL)
FV(5) = F3T(LVL)
AREST = ARESTT(LVL)
CEST = CESTT(LVL)
EFS = EFS(T(LVL)
GC TO 1 2
IFLAG = 2
5 GC TO 2 3
6 IFLAG = 2
GC TO 2
END
COMPLEX FUNCTION Q1DAIP*16(DK,DR,DW,RHO,CFS1,SGMA,XSTN,Q1CF,N,IPT)
IMPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX * 16 (Q,Z)
DIMENSION Q1CF(13)
IF (IPT.GT.0) WRITE(6,990) DK,DR,FW,RHO,OFST,SGMA,XSTN,IPT
IF (IPT.GT.0) Q1CAIP = Q1CF(13)
FCR MAT(0,10X,'DR',11X,'CH',11X,'RHO',10X,'CFS1',9X,'SGMA',9X,
1,10X,'9X',IPT,/,
2,XSTN,XSTN-OFST
XSTN = XSTN - OFST
IF (XASTN.LE.DR+RHO-1.0D0) GC TC 20
ICT = IPT - 1
GCCNST = CCPLX(0.0D0,SGMA)
A = DR-1.0D0
E = XASTN - RHO - 1.0D-8
CALL Q1DZSM(DK,DR,DW,RHO,XSTN,A,B,N,QANS,Q1CF,IOT)
Q1CAIP = QANS
IF (IPT.LE.0) RETURN
GC TO 60
2C Q1DAIP = DCPLX(0.0D0,0.0D0)
IF (IPT.LE.0) RETURN
60 WRITE(6,995) Q1DAIP
995 FCR MAT(0,10X,'Q1CAIP = ',E14.7,' ',E14.7)
RETURN
END
COMPLEX FUNCTION Q1DRIP*16(DK,DF,DW,RHO,OFFSET,XSTN,Q1CF,N,IPT)
IMPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX * 16 (C,Z)
DIMENSION Q1CF(13)

```


CLDR7205
QLDR7210
CLDR7215
QLDR7220
CLDR7225
QLDR7230
CLDR7235
QLDR7240
CLDR7245
QLDR7250
CLDR7255
QLDR7260
CLDR7265
QLDR7270
CLDR7275
QLDR7280
CLDR7285
QLDR7290
CLDR7295
QLDR7300
CLDR7305
QLDR7310
CLDR7315
QLDR7320
CLDR7325
QLDR7330
CLDR7335
QLDR7340
CLDR7345
QLDR7350
CLDR7355
QLDR7360
CLDR7365
QLDR7370
CLDR7375
QLDR7380
CLDR7385
QLDR7390
CLDR7395
QLDR7400
CLDR7405
QLDR7410
CLDR7415
QLDR7420
CLDR7425
QLDR7430
CLDR7435
QLDR7440

```

IF (IPT.GT.0) WRITE(6,990) CK,DR,DW,RHO,XSTN,IPT
FCRMT(0,10X,1Q1DRIF,ENTERED WITH:,,/,
1CX,DK,11X,1CR,11X,DW,11X,RHO,10X,
XSTN,9X,IPT,/,10X,5(E12.5),I3)
IF(XSTN.LE.CR+RHO+OFFSET-1.0D0) GOTO 20
ICT = IPT - 1
A = DR-1.0D0
B = XSTN - RHO - 1.0D-8
CALL Q1DZSM(CK,DR,CW,RHO,XSTN,A,B,N,QANS,Q1CF,IOT)
Q1CRIP = -QANS
IF(IPT.LE.0) RETURN
GOTO 60
20 Q1CRIP = DCPLX(0.0D0,0.0D0)
60 IF (IPT.LE.0) RETURN
955 WRITE(6,995) Q1DRIF
FCRMT(0,10X,Q1CRIP = ,E14.7,/,E14.7)
RETURN
END
SUBROUTINE Q1DZSM (DK,DR,DW,RHO,XSTN,A,B,J,QANS,Q1CF,IPT)
IMPLICIT REAL*8(A - E,G,H,M,C,P,F - Y), COMPLEX*16(F,Q,Z)
DIMENSION Q1CF(13)
DIMENSION FV(5),LCRR(60),F2T(60),F3T(60),DAT(60),
1ARESTT(60),QESTT(60),EPST(60),CPSUM(60)
1F(X) = GLGNCR(X,CR,J,Q1CF)*CDEXP*(X)
1*OMEGA * DSQRT((XSTN-X)*(XSTN-X) - YY)), IER)
2*OMEGA * ((XSTN-X)/(DSQRT((XSTN-X)*(XSTN-X)-YY))
GAMMA = 1.4D0
YY = RHO * RHO
CM2 = (GAMMA + 1.0D0) * CW
OMEGA = DSQRT (DK*DK*(1.0D0-DM2)/(CM2*DM2))
CLAMDA = DK/DM2
CM = DSQRT(CM2)
Q2EXP = CDEXP (DCMFLX (0.0D0, -CLAMDA*XSTN))
QEXP = CCPLX(0.0D0,CLAMDA)
U = 9.0D-13
ACC = 1.0D-6
IF (IPT.GT.0) WRITE(6,990)DK,DR,CW,RHO,XSTN,A,B,J,IPT
FCRMT(0,15X,1Q1DZSM,ENTERED WITH ARGUMENTS:,,/,
1,15X,DK,15X,DR,13X,DW,
2A,14X,B,14X,J,2X,IPT,/,
3,15X,7(E14.7,/,I2,2X,I3)
EFCURU = 4.C*U
IFLAG = 1
EPS = ACC
GEFRROR = DCPLX(0.0D0,0.0D0)
LVL = 1
LCFR(LVL) = 1
QPSUM(LVL) = 0.0

```


Q LDR7445
 Q LDR7450
 Q LDR7455
 Q LDR7460
 Q LDR7465
 Q LDR7470
 Q LDR7475
 Q LDR7480
 Q LDR7485
 Q LDR7490
 Q LDR7495
 Q LDR7500
 Q LDR7505
 Q LDR7510
 Q LDR7515
 Q LDR7520
 Q LDR7525
 Q LDR7530
 Q LDR7535
 Q LDR7540
 Q LDR7545
 Q LDR7550
 Q LDR7555
 Q LDR7560
 Q LDR7565
 Q LDR7570
 Q LDR7575
 Q LDR7580
 Q LDR7585
 Q LDR7590
 Q LDR7595
 Q LDR7600
 Q LDR7605
 Q LDR7610
 Q LDR7615
 Q LDR7620
 Q LDR7625
 Q LDR7630
 Q LDR7635
 Q LDR7640
 Q LDR7645
 Q LDR7650
 Q LDR7655
 Q LDR7660
 Q LDR7665
 Q LDR7670
 Q LDR7675
 Q LDR7680

```

ALPHA = A
DA = B - A
AREA = 0.0
AREST = 0.0
FV(1) = F(ALPHA)
FV(3) = F(ALPHA + 0.5*DA)
FV(5) = F(ALPHA + DA)
KCUNT = 3
WT = DA/6.0
CEST = WT*(FV(1) + 4.0*FV(3) + FV(5))
DX = 0.5*DA
FV(2) = F(ALPHA + 0.5*DX)
FV(4) = F(ALPHA + 1.5*DX)
KCUNT = KOUNT + 2
WT = DX/6.0
CESTL = WT*(FV(1) + 4.0*FV(2) + FV(3))
CESTR = WT*(FV(3) + 4.0*FV(4) + FV(5))
QSUM = CESTL + CESTR
ARESTL = WT*(CDABS(FV(1)) + CDABS(4.0*FV(2)) + CDABS(FV(3)))
ARESTR = WT*(CDABS(FV(3)) + CDABS(4.0*FV(4)) + CDABS(FV(5)))
AREA = ARESTL + ARESTR - AREST
QDIFF = CEST - QSUM*EPS*DABS(AREA) GO TO 2
IF(CDABS(DX).LE.EFCURU*DABS(ALPHA)) GO TO 5
IF(LVL.GE.60) GO TC 5
IF(KCUNT.GE.4000) GO TO 6
LVL = LVL + 1
LCRR(LVL) = 0
F1T(LVL) = FV(3)
F2T(LVL) = FV(4)
F3T(LVL) = FV(5)
DX = DX
DAT(LVL) = DX
ARESTL = ARESTL
ARESTR = ARESTR
CESTL = CESTL
CESTR = CESTR
EPS = EPS/1.4
EPST(LVL) = EPS
FV(5) = FV(3)
FV(3) = FV(2)
GC TC 1
GERRCR = GERROR + CDIFF/15.0
IF(LCRR(LVL).EQ.0) GO TO 4
QSUM = QPSUM(LVL) + QSUM
LVL = LVL - 1
IF(LVL.GT.1) GO TC 2
GANS = (QLGNDR(B,CR,J,QICF)*CDEXF(CEXP*B) - QSUM)*Q2EXP/DM
  
```

1

2 3

5
 76890
 76950
 77000
 77100
 77150
 77200
 77250
 77300
 77350
 77400
 77450
 77500
 77550
 77600
 77650
 77700
 77750
 77800
 77850
 77900
 77950
 78000

7. Gorelov Spanning Function.

The subprogram for function used by Gorelov is shown below.

```
REAL FUNCTION PLGNDR*8(X,DR,N)
IMPLICIT REAL*8(A-T,C-Z)
IF(N.EQ.0) GOTO 100
ETA = CARCCS(-X)
ETASTR = DARCOS(1.000 - DR)
FN = CFLCAT(N)
PLGNDR = DCCS(FN*ETA)-DCOS(FN*ETASTR)
RETURN
100 PLGNDR = 1.000
RETURN
END
```


8. Linear Expansion Program

The program based on the linear expansion for small k is shown below.


```

C      IMPLICIT REAL*8(A-H,O,P,R-Y), CCMFLEX*16(Q,Z)
C      DIMENSION X(13), Q2PT(13), Q2CP(13)
C      BLOCK ONE READ AND EDIT DATA
C      CALL ERRSET(208,256,-1,1)
C      WRITE(6,910)
C      CALL READ(DK,DR,DW,RHO,OFFSET,SIGMA,N,NF,IPT)
C      IF(IPT.GT.0)WRITE(6,990)DK,DR,DW,SIGMA,OFFSET,RHO,N,NF
C      910 FCRMAT(1,1,5X,'GORELCV CASCADE PROGRAM LINEARIZED FOR SMALL DK')
C      990 FCRMAT(1,0,5X,'INPUT VALUES TRANSMITTED TO MAIN PROGRAM:',/,
C      1,1,10X,'DK',13X,'CR',13X,'DW',10X,'SIGMA',10X,'OFFSET',/,
C      1,1,10X,'RHO',12X,'N',5X,'NFCN',
C      2,0,10X,'RHO',12X,'N',5X,'NFCN',
C      3,/,1,10X,'1(E12.5,3X)',12,4X,I2)
C      CALL ABSA(N,OFFSET,X,RHO,DW)

C      BLOCK TWO CALLS CALCULATION ROUTINES FOR ZONE ONE AND ZONE TWO
C      CALL Q$CNE(DK,DR,DW,RHO,OFFSET,SIGMA,N,NF,IPT,X)
C      GO TO 1
C      END
C      SUBROUTINE READ (DK,DR,DW,RHO,CFFSET,SIGMA,N,NF,IPT)
C      IMPLICIT REAL*8(A-H,C,P,R-Y)
C      READ(5,905) DK,DR,DW,RHO,OFFSET,SIGMA,N,NF,IPT
C      IF (DK.LT.0.000) STOP
C      IF (IPT.GT.C) WRITE(6,910)
C      GAMMA = 1.400
C      DR = RHP * DSQRT((GAMMA + 1.000) * DW)
C      RHO = DR
C      IF(N.LE.2) GO TO 1
C      N = 2
C      WRITE(6,935)
C      1 IF(OFFSET.LE.1.900) GO TO 2
C      910 FCRMAT(6,940)
C      CFFSET = OFFSET-1.000
C      GO TO 1
C      2 CCNTINUE
C      IF(IPT.GT.0) WRITE(6,925) DK,DR,DW,SIGMA,CFFSET,RHO,N,NF,IPT
C      RETURN
C      905 FCRMAT(6,910-4,3I2)
C      910 FCRMAT(1,1,10X,'GORELOV SLIGHTLY SUPERSONIC CASCADE PROGRAM',/,
C      1,15X,'LINEARIZED FOR SMALL FREQUENCY, DK',
C      925 FCRMAT(1,0,10X,'CK',13X,'DR',13X,'DW',10X,'SIGMA',10X,'OFFSET',
C      1,/,1,10X,'1(E12.5,3X)',/,
C      2,1,10X,'RHO',12X,'N',5X,'NFCN',2X,'IPT',
C      3,/,1,10X,'1(E12.5,3X)',12,4X,I2,4X,I2)
C      935 FCRMAT(1,0,5X,'ORIGINAL N TCC LAFGE (.GT.13) - RESET TO N = 13')
C      940 FCRMAT(1,0,5X,'OFFSET TOO LARGE (.GT.1.9), RESET AS OFFSET =
C      1000010
C      1000020
C      1000030
C      1000040
C      1000050
C      1000060
C      1000070
C      1000080
C      1000090
C      1000100
C      1000110
C      1000120
C      1000130
C      1000140
C      1000150
C      1000160
C      1000170
C      1000180
C      1000190
C      1000200
C      1000210
C      1000220
C      1000230
C      1000240
C      1000250
C      1000260
C      1000270
C      1000280
C      1000290
C      1000300
C      1000310
C      1000320
C      1000330
C      1000340
C      1000350
C      1000360
C      1000370
C      1000380
C      1000390
C      1000400
C      1000410
C      1000420
C      1000430
C      1000440
C      1000450
C      1000460
C      1000470
C      1000480

```


LIN0049C
 LIN00500
 LIN00510
 LIN00520
 LIN00530
 LIN00540
 LIN00550
 LIN00560
 LIN00570
 LIN0058C
 LIN00590
 LIN0060C
 LIN00610
 LIN00620
 LIN0063C
 LIN00640
 LIN00650
 LIN0066C
 LIN00670
 LIN00680
 LIN00690
 LIN00700
 LIN0071C
 LIN00720
 LIN0073C
 LIN00740
 LIN00750
 LIN00760
 LIN00770
 LIN00780
 LIN00790
 LIN00800
 LIN00810
 LIN00820
 LIN00830
 LIN00840
 LIN0085C
 LIN00860
 LIN00870
 LIN0088C
 LIN00890
 LIN00900
 LIN0091C
 LIN00920
 LIN0093C
 LIN00940
 LIN00950
 LIN00960

```

END
SUBROUTINE ABSA (N,OFFSET,X,DR,DW,
)
IMPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX*16(Q,Z)
DIMENSION X(13)
XINT = (2.000-DR)/CFLOAT(N+1)
XL = CR - 1.000 + 1.00-8
DO 10 I = 1,N
  X(I) = XL + (XINT*DFLOAT(I))
  IF(X(I).EQ.0.000) X(I) = .10-14
10 CONTINUE
RETURN
END
SUBROUTINE Q$ONE(DK,DR,DW,RHO,OFFSET,SIGMA,N,NF,IPT,X)
IMPLICIT REAL*8(A-H,C,P,R-Y), COMPLEX*16(Z,C)
DIMENSION Q1COF(26), Q1INT(26,26), Q1RBP(13), Q1ABP(13)
DIMENSION Q1RBCF(13), Q1ABCF(13)
DIMENSION X(13)
IPT = IPT - 1
IF(IPT.GT.0)WRITE(6,990)DK,DR,RHO,CFFSET,SIGMA,N,NF,IPT
990 FORMAT(0, SUBROUTINE Q$ONE ENTERED WITH: ',/,
1, ',5X,'DK',13X,'CR',13X,'RHO',12X,'OFFSET',9X,'SIGMA',10X,
2, ',N',3X,'NF',3,2X,'/',
3, '5X,5(E12.5,3X),12,2X,I2,2X,I3)
CALL Q1ZINT(DK,DR,DW,RHO,OFFSET,SIGMA,N,X,ICT,Q1CCF,Q1INT)
CALL Q1COEF(Q1COF,Q1INT,N,IPT,Q1ABCF,Q1RBCF)
CALL Q1PPOT(DK,DR,DW,RHO,OFFSET,SIGMA,N,X,Q1AECF,Q1RBCF,ICT)
IOUT = 0
CALL Q1CCOF(DK,DR,DW,RHO,OFFSET,SIGMA,N,Q1AECF,Q1RBCF,ICT)
RETURN
END
C
C
C
SUBROUTINE Q1ZINT(DK,DR,DW,RHO,CFFSET,SIGMA,N,X,
IPT,Q1COF,Q1INT)
IMPLICIT REAL*8(A-H,O,P,R-Y), COMPLEX * 16(Z,Q)
DIMENSION Q1COF(26), Q1INT(26,26), Q1INTRP(13), Q1INTAP(13)
DIMENSION X(13)
FCRMAT(0,10X,'Q1ZINT ENTERED WITH: ',/,
1, ',10X,'DK',13X,'DR',13X,'RHO',12X,'OFFSET',9X,'SIGMA',10X,
2, ',N',2X,'IPT',/,
3, ',10X,5(E12.5,3X),I2,2X,I3)
QCONST = CDEXP(DCMPLX(0.000,SIGMA))
IF (IPT.GT.0) WRITE (6,990) DK,DR,RHO,OFFSET,SIGMA,N,IPT
ICT = IPT - 1
GAMMA = 1.400
CLAMDA = DK/((GAMMA+1.000)*DW)
DO 90 I = 1,N
990

```



```

IN = I + N
XSTN = X(I) - DR
XCP = CDEXP(DCMPLX(C.0D0, DLAMDA*XSTN))
CALL Q1CABP(DK, DR, CW, RHO, OFFSET, SIGMA, XSTN, CINTAP, N, IOT)
CALL Q1CRIP(DK, DR, DW, RHC, OFFSET, XSTN, QINTRP, N, ICT)
DO 20 J = 1, N
  JN = N + J
  J1 = J - 1
  Q1INT(I, 1) = DCMPLX(1.0D0, CLAMDA*XSTN)
  TEMP = CR-XSTN-1.0D0
  Q1INT(I, 2) = DCMPLX(TEMP, CLAMDA*XSTN*TEMP)
  Q1INT(IN, J) = QINTRP(J)
  Q1INT(I, JN) = QINTAP(J)
  XASTN = XSTN - OFFSET
  Q1INT(IN, 3) = DCMPLX(1.0D0, DLAMDA*XASTN)
  TEMP = DR-XASTN-1.0D0
  Q1INT(IN, 4) = DCMPLX(TEMP, DLAMDA*XASTN*TEMP)
  CCNTINUE
20  Q1CCF(IN) = -Q1CRBP(DK, DR, DW, RHO, XSTN, IOT)
  Q1CCF(I) = -Q1CABP(DK, DR, DW, RHC, CFFSET, SIGMA, XSTN, IOT)
  CCNTINUE
90  CONTINUE
  ENCL
  COMPLEX FUNCTION Q1CRBP*16(DK, DF, DW, RHO, XSTN, IPT)
  IMPLICIT REAL*8 (A-H, O, P, R-Y), COMPLEX*16 (Q, Z)
  DIMENSION QINP(2)
  IF (IPT.GT.0) WRITE(6, 990) CK, CR, CW, RHO, XSTN, IPT
  FCRMAT(0, 10X, 'Q1CRBP ENTERED WITH: ', /,
1    , 10X, 'DK, 11X, 'CR, 11X, 'DW, 11X, 'RHO', 10X, 'XSTN', 9X, 'IPT',
2    , 10X, '10X, 5(E12.5, ', 13)
  IF(XSTN.LE.RHO-1.0D0) GOTO 20
  IF(XSTN.GT.2.0D0) GOTO 20
  ICT = IPT - 1
  QCK = DCMPLX(0.0D0, CK)
  GAMMA = 1.4D0
  CLAMDA = DK/((GAMMA+1.0D0)*DW)
  Q1CRBP = DCMPLX(1.0D0, (DK+DLAMDA)*(XSTN-DR))
  IF(IPT.LE.0) RETURN
  GOTO 30
20  Q1CRBP = DCMPLX(0.0D0, 0.0D0)
  IF(IPT.LE.0) RETURN
30  WRITE(6, 995) Q1CRBP
995  FORMAT('C', 10X, 'Q1CRBP = ', E14.7, ', ', E14.7)
  RETURN
  ENCL
  COMPLEX FUNCTION Q1CABP*16(CK, DR, CW, RHO, OFFSET, SIGMA, XSTN, IPT)
  IMPLICIT REAL*8 (A-H, O, P, R-Y), COMPLEX*16 (Q, Z)

```

```

LIN0057C
LIN0058C
LIN0059C
LIN01000
LIN01010
LIN01020
LIN01030
LIN0104C
LIN01050
LIN0106C
LIN01070
LIN0108C
LIN0109C
LIN0110C
LIN0111C
LIN01120
LIN0113C
LIN01140
LIN01150
LIN01160
LIN01170
LIN01180
LIN01190
LIN0120C
LIN01210
LIN01220
LIN01230
LIN0124C
LIN01250
LIN01260
LIN01270
LIN01280
LIN01290
LIN01300
LIN01310
LIN01320
LIN01330
LIN01340
LIN01350
LIN01360
LIN01370
LIN0138C
LIN01390
LIN01400
LIN0141C
LIN01420
LIN01430
LIN01440

```



```

CJMENSICN QINP(2)
IF(IPT.GT.0) WRITE(6,990) DK,DR,DW,RHO,OFFSET,SIGMA,XSTN,IPT
FORMAT(0,'10X',Q1CABP,ENTERED WITH:','/,
1  '10X',CK,11X,DR,11X,DW,11X,RHO,10X,OFFSET',7X,
2  'SIGMA',8X,XSTN,9X,IPT,/,',10X,7(E12.5,',',),13)
XASTN = XSTN - OFFSET
IF(XASTN.LE.RHO-1.000) GOTO 20
IF(XASTN.GT.2.000) GOTO 20
IPT = IPT - 1
QCK = DCMLPX(0.000,DK)
CCONST = CDEXP( DCMLPX(0.000, SIGMA))
GAMMA = 1.400
DLAMDA = CK/((GAMMA+1.000)*DW)
Q1CABP = DCMLPX(1.000,(DK+DLAMDA)*((XASTN-[R]))*QCONST
IF(IPT.LE.0) RETURN
GC TO 30
20 Q1CABP = DCMLPX(C.000,0.000)
IF(IPT.LE.0) RETURN
30 WRITE(6,995) Q1CABP
995 FORMAT(0,'10X',Q1CABP = ',E14.7,',',E14.7)
RETURN
END
SUBROUTINE Q1CAIP(CK,DR,DW,RHO,CFST,SGMA,XSTN,QCAIP,N,IPT)
IMPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX * 16 (C,Z)
DIMENSION QINP(13),QCAIP(13)
IF(IPT.GT.0) WRITE(6,990) CK,DR,DW,RHO,CFST,SGMA,XSTN,IPT
FCRMAT(0,'10X',Q1CAIP,ENTERED WITH:','/,
1  '10X',CK,11X,DR,11X,DW,11X,RHO,10X,OFST',9X,SGMA',9X
2  'XSTN',9X,IPT,/,',10X,7(E12.5,',',),13)
XASTN = XSTN - CFST
IF(XASTN.LE.DR+RHC-1.000) GO TO 20
IF(XASTN.GT.2.000) GOTO 20
ICT = IPT - 1
QCCNST = CDEXP( DCMLPX(0.000,SGMA))
GAMMA = 1.400
DLAMDA = CK/((GAMMA+1.000)*DW)
QCAIP(1) = DCMLPX(1.000,DLAMDA*(XASTN-RHC))
TEMP = DR+RHO-XASTN-1.000
QCAIP(2) = DCMLPX(TEMP,DLAMDA*(XASTN-RHO)*TEMP)
IF(IPT.LE.0) RETURN
GOTO 30
20 ZERO = DCMLPX(0.000,0.000)
DC 25 I = 1,N
QCAIP(I) = ZERO
QCCNTINUE
25 IF(IPT.LE.0) RETURN
30 WRITE(6,995)
995 FCRMAT(0,'0',10X,'Q1CAIP RESULTS: J QCAIP(J)')

```



```

DC 40 J = 1,N
WRITE (6,996) J,CCAIP(J)
FCRPMAT(0,26X,I2,3X,E14.7,.,,E14.7)
CONTINUE
4C RETURN
END
SUBROUTINE CCRIP (OK,DR,DK,RHO,CFFSET,XSTN,CCRIP,N,IPT)
IMPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX * 16 (Q,Z)
DIMENSION CCRIP(13)
IF (IPT.GT.0) WRITE(6,990) DK,DR,CK,RHO,XSTN,IPT
FCRPMAT(0,10X,CCRIP ENTERED WITH:./,
1 .,10X,CK,11X,DR,11X,CK,11X,RHC,1CX,
2 .,XSTN,9X,IPT,./,10X,5(E12.5,.,),I3)
IF(XSTN.LE.DR+RHO+CFFSET-1.0CO) GO TO 20
IF(XSTN.GT.2.0DO) GO TO 20
IPT = IPT - 1
GAMMA = 1.4CO
DLAMDA = DK/((GAMMA+1.0CO)*DW)
CCRIP(1) = CCPLX(1.0DO,DLAMDA*(XSTN-RHO))
TEMP = DR+RHO-XSTN-1.0DO
CCRIP(2) = DCPLX(TEMP,DLAMDA*(XSTN-RHO)*TEMP)
IF(IPT.LE.0) RETURN
GO TO 30
ZERO = CCPLX(0.0DO,0.0DO)
DC 25 I = 1,N
CCRIP(I) = ZERO
25 IF (IPT.LE.0) RETURN
30 WRITE (6,995)
595 FCRPMAT(0,10X,CCRIP RESULTS: J CCRIP(J),)
DC 40 J = 1,N
WRITE (6,996) J,CCRIP(J)
FCRPMAT(0,26X,I2,3X,E14.7,.,,E14.7)
CONTINUE
4C RETURN
END
SUBROUTINE GLCOEF( QICOF,Q1INT,N,IPT,Q1ABCF,Q1RBCF)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX * 16 (Z,Q)
DIMENSION QICOF(26), Q1INT(26,26), ZWA(300)
DIMENSION Q1ABCF(13), Q1RBCF(13)
IF (IPT.GE.0) WRITE (6,90)
IB = 26
M2 = 1
N2 = 1
N2 = 2*N
IF (IPT.LE.0) GO TO 5
WRITE (6,98) N,N2
FCRPMAT(0,5X,Q1COEF ENTERED WITH ,I2, DEG PWR SERIES (,I2,
58 1, SQUARE MATRIX),)
1 CC 2 I = 1,N2

```

LIN0193C
 LIN01940
 LIN01950
 LIN01960
 LIN01970
 LIN01980
 LIN01990
 LIN02000
 LIN02010
 LIN02020
 LIN02030
 LIN02040
 LIN02050
 LIN02060
 LIN02070
 LIN02080
 LIN02090
 LIN02100
 LIN02110
 LIN02120
 LIN02130
 LIN02140
 LIN02150
 LIN02160
 LIN02170
 LIN02180
 LIN02190
 LIN02200
 LIN02210
 LIN02220
 LIN02230
 LIN02240
 LIN02250
 LIN02260
 LIN02270
 LIN02280
 LIN02290
 LIN02300
 LIN02310
 LIN02320
 LIN02330
 LIN02340
 LIN02350
 LIN02360
 LIN02370
 LIN02380
 LIN02390
 LIN02400


```

WRITE(6,92) I, I, QICOF(I)
FORMAT(0,10X,QICCEF EQUATION SYSTEM, ROW ,I2,/,
1,10X,QICOF(I2)) = ,E14.7,,E14.7)
CC 2 J = 1,N
J2=J+N
WRITE(6,91) I,J,CLINT(I,J),I,J2,CLINT(I,J2)
FCRMTAT(,15X,2,QINT(,I2,,I2,,E14.7,,E14.7,10X))
CCNTINUE
IA = 26
IJOB=0
LECTIC(QIINT,N2,IA,QICCF,M,IE,IJOB,ZHA,IER)
CALL LER(EQ,0) GOTC 30
IF(IER.EQ.0) GOTC 30
IF(IER.EQ.129) GC TO 10
WRITE(6,93)
FCRMTAT(,C,10X,QICCEF - ITERATIVE IMPROVEMENT FAILED, MATRIX TOO
1ILL-CONDITIONED. USE RESULTS WITH CAUTION.)
GC TO 30
WRITE(6,95)
FORMAT(0,10X,QICCOEF - MATRIX ALGORITHMICALLY SINGULAR. CCEFFIC
1IENTS SET TO ZERO.)
ZERC = CCPLX(0.0C0,C.000)
CC 20 I = 1,N
I2 = I+N
QICOF(I) = ZERO
QICCF(I2) = ZERO
CCNTINUE
CC 35 I = 1,N
IN = I + N
QIABCF(I) = QICOF(IN)
QIRBCF(I) = QICOF(I)
CCNTINUE
IF(IPT.LE.0) RETURN (6,94)
IF(IPT.GE.C) WRITE (6,94)
CC 40 I = 1,N
IM1 = I-1
WRITE(6,99) I, IM1, QIRBCF(I), QIABCF(I)
CCNTINUE
FCRMTAT(,0,5X,I2,10X,I2,10X,2(E14.7,5X,E14.7,10X))
FCRMTAT(,C,10X,SUBROUTINE QICCEF - COMPLEX POWER SERIES CCEFFIC
1IENTS)
FCRMTAT(,0,5X,INDEX,7X,DEG FCLY,4X,REFERENCE BLADE TERMS GIC
3CCF(INDEX),7X,ADJACENT BLADE TERMS QICCF(2*INDEX))
ENCL
SUBROUTINE QIPROT(DK,DR,DW,RHO,CFFSET,SIGMA,N,X,QIABCF,QIRBCF,IPT)
IMPLICIT REAL * 8(A-H,O,P,R-Y), COMPLEX * 16(Z,Q)
DIMENSION QIABCF(13), QIRBCF(13), CRR(13), CAA(13), CPHI(13)

```



```

WRITE (6,95) I,XSTN
WRITE (6,91) CDR,QCRO,CDAP,QCRIPO,CCAIPP
WRITE (6,92) CCA,QCRP,CDAO,QDRIPI,CCAIPQ
CCRR(I) = CCR
QCAA(I) = QCA
FCRMAI (,O X-STATICN NUMBER ,I2, , XSTN = ,F6.4,/,
1. BL TOTAL D(PCT)/DX, ,14X, ,REF EL D(POT)/DX, ,8X,
2. ,ADJ BL D(POT)/DX, ,8X, ,REF BL INT D(POT)/CX, ,5X,
3. ,ADJ BL INT D(POT)/DX, )
1C CCATINUE
WRITE (6,954)
954 FCRMAI (,I, ,10X, ,SUMMARY LISTING,/,
1. C, ,10X, ,XSTN, ,7X, ,SINGLE BLADE TOTAL POTENTIAL, ,6X,
1. ,REF ELADE POTENTIAL, ,15X, ,ADJ ELADE POTENTIAL, )
DC 20 I = 1, N
XSTN = X(I)
WRITE (6,94) XSTN,CPHI(I),QCR(I),CAAI(I)
94 FCRMAI (, , ,10X, ,F6.4,3(5X,E14.7, , , ,E14.7) )
20 CCATINUE
WRITE (6,996)
956 FCRMAI (,O, ,10X, ,XSTN, ,7X, ,SINGLE ELADE TOTAL C(POT)/CX, ,6X,
1. ,REF ELADE D(POT)/DX, ,15X, ,ADJ ELADE D(POT)/DX, )
DC 50 I = 1, N
XSTN = X(I)
WRITE (6,94) XSTN,CDPHI(I),QCR(I),CDAI(I)
5C CCATINUE
RETURN
END
SUBROUTINE CIDCOF (CK,DR,DW,RHO,CFFSET,SIGMA,N,QIABCF,QIRBCF,IPT)
IMPLICIT REAL * 8 (A-F,O,P,R-Y), COMPLEX * 16 (Q,Z)
DIMENSION QIABCF(13), QIRBCF(13)
IF (IPT.GT.0) WRITE (6,990) DK,DR,DW,RHO,OFFSET,SIGMA,N,IPT
FCRMAI (,I, ,10X, ,QIDCOF - CALCULATION OF COMPLEX DIMENSIONLESS AERC
1. DYNAMIC CEFFICIENTS,/,
3. ,O, ,10X, ,DK, ,13X, ,DR, ,13X, ,DW, ,13X, ,RHO, ,12X, ,OFFSET, ,5X, ,SIGMA,
4. , ,10X, ,N, ,3X, ,IPT, ,/, , ,10X,
5. (E12.5,3X),I2,2X,I3)
ICT = IPT - 3
ICCL = ICCL(DK,DR,DW,RHO,OFFSET,SIGMA,N,QIABCF,QIRBCF,IOT)
GCCM = QIDCM(DK,DR,DW,RHO,OFFSET,SIGMA,N,QIABCF,QIRBCF,IOT)
GAMMA = 1.4CO
TAU = (2.0DO*DSQRT((GAMMA + 1.0CO)*DW))/DR
WRITE (6,90) DK,TAU,DW,N,SIGMA,CCCL,QDCM
FCRMAI (,O, ,5X, ,DK = ,F6.3, , ,TAU = ,F7.4, , ,DW = ,F6.3, , ,N =
1. I2, , ,SIGMA = ,F6.3, , ,CL = ,F9.4, , ,CM = ,
2. F9.4, , ,F9.4)
END
RETURN
END

```



```

CCOMPLEX FUNCTION C1DCL*16(DK,DR,CW,RHO,OFFSET,SIGMA,N,Q1ABCF,CIRBCF,CIRBCLIN038550
IF,IPLT) IT REAL*8(A - E,G,F,O,P,R - Y), COMPLEX*16(F,Q,Z) LIN038760
IAPPLICATION Q1ABCF(13),QIRBCF(13) LIN038870
DIMENSION FV(5),F1T(60),F3T(60),CESTT(60),CPSUM(60) LIN038980
DIMENSION DAT(60),ARESTT(60),EPST(60) LIN039090
DIMENSION LCRR(60)} LIN039200
F(X) = (QIDPHI(DK,DR,CW,RHO,OFFSET,SIGMA,N,C1ABCF,CIRBCF,X,ICT) LIN039310
-QALPHA*C1PHI(CK,DR,DW,RHG,OFFSET,SIGMA,N,C1ABCF,CIRBCF,X,ICT)) LIN039420
1 IF (IPT.GT.C) WRITE(6,990) DK,DR,CW,RHG,CFFSET,SIGMA,N,IPT LIN039530
FCRMAT(0,10X,13X,'Q1DCL ENTERED WITH:',/, LIN039640
,10X,'DK',13X,'DR',13X,'DK',13X,'RHO',12X,'OFFSET',5X,'SIGMA' LIN039750
,10X,'N',3X,'IPT',/,10X, LIN039860
56{E12,5,3X},12,2X,13} LIN039970
A = -1.000 LIN040080
B = 1.000 LIN040190
ICT = IPT - 1 LIN040300
GAMMA = 1.400 LIN040410
LLAMDAA = DK/(GAMMA + 1.000) * CW LIN040520
CALPHA = CCMLPX(0.000,DLAMDAA-DK) LIN040630
U = 9.0E-13 LIN040740
ACC = 1.00E-5 LIN040850
EFFCURU = 4.0*U LIN040960
IFLAG = 1 LIN041070
EPS = ACC LIN041180
QERROR = DCMLPX(0.000,0.000) LIN041290
LVL = 1 LIN041400
LCRR(LVL) = 1 LIN041510
CFSUM(LVL) = 0.0 LIN041620
ALPHA = A LIN041730
DA = B - A LIN041840
AREA = 0.0 LIN041950
AREST = 0.0 LIN042060
FV(1) = F(ALPHA) + 0.5*CA LIN042170
FV(3) = F(ALPHA) + CA LIN042280
FV(5) = F(ALPHA) LIN042390
KCUNT = 3 LIN042500
WT = DA/6.0 LIN042610
CEST = WT*(FV(1) + 4.0*FV(3) + FV(5)) LIN042720
DX = 0.5*DA LIN042830
FV(2) = F(ALPHA) + C.5*DX LIN042940
FV(4) = F(ALPHA) + 1.5*DX LIN043050
KCUNT = KCUNT + 2 LIN043160
WT = DX/6.0 LIN043270
CESTL = WT*(FV(1) + 4.0*FV(2) + FV(3)) LIN043380
QUESTR = WT*(FV(3) + 4.0*FV(4) + FV(5)) LIN043490
QSUM = QUESTL + CESTR LIN043600
ARESTL = WT*(CDABS(FV(1)) + CDABS(4.0*FV(2)) + CDABS(FV(3))) LIN043710

```



```

ARESTR = WT*(CDABS(FV(3)) + CCABS(4.0*FV(4)) + CDABS(FV(5)))
AREA = AREA + ((ARESTL + ARESTR) - AREST)
QDIFF = QUEST - QSUM
IF(CCABS(QDIFF).LE.EPS*DABS(AREA))GO TO 2
IF(DABS(DX).LE.EFCURU*DABS(ALPHA))GO TO 5
IF(LVL.GE.60)GO TO 5
IF(KCUNT.GE.4000)GO TO 6
LVL = LVL + 1
LCRR(LVL) = 0
F1T(LVL) = FV(3)
F2T(LVL) = FV(4)
F3T(LVL) = FV(5)
CX = CX
DAT(LVL) = DX
AREST = ARESTL
ARESTT(LVL) = ARESTR
QUESTT(LVL) = QUEST
EPS = EPS/1.4
EPST(LVL) = EPS
FV(1) = FV(2)
FV(3) = FV(2)
GC TO 1
CERROR = QERROR + QDIFF/15.0
IF(LORR(LVL).EQ.0)GO TO 4
QSUM = QPSUM(LVL) + QSUM
LVL = LVL - 1
IF(LVL.GT.1)GO TO 3
Q1DCL = QSUM * 2.0C0
IF(IPT.GT.0)GO TO 11
IF(IFLAG.EQ.1)RETURN
WRITE(6,990) DK,DR,DH,RHO,OFFSET,SIGMA,N,IPT
990 FORMAT(15X,'Q1DCL = ',E14.7,/,
1,15X,'IFLAG',2X,'QERROR',/,
2,15X,'I3,2X,E14.7,15X,E14.7)
RETURN
QPSUM(LVL) = QSUM
LCRR(LVL) = 1
ALPHA = ALPHA + DA
DA = DAT(LVL)
FV(1) = FIT(LVL)
FV(3) = F2T(LVL)
FV(5) = F3T(LVL)
AREST = ARESTT(LVL)
EPS = EPST(LVL)
GC TO 1

```

2 3

11 990

4

LIN04330
 LIN04340
 LIN04350
 LIN04360
 LIN04370
 LIN04380
 LIN04390
 LIN04400
 LIN04410
 LIN04420
 LIN04430
 LIN04440
 LIN04450
 LIN04460
 LIN04470
 LIN04480
 LIN04490
 LIN04500
 LIN04510
 LIN04520
 LIN04530
 LIN04540
 LIN04550
 LIN04560
 LIN04570
 LIN04580
 LIN04590
 LIN04600
 LIN04610
 LIN04620
 LIN04630
 LIN04640
 LIN04650
 LIN04660
 LIN04670
 LIN04680
 LIN04690
 LIN04700
 LIN04710
 LIN04720
 LIN04730
 LIN04740
 LIN04750
 LIN04760
 LIN04770
 LIN04780
 LIN04790
 LIN04800

5 IFLAG = 2
 6 GC TO 2 3
 GC TO 2

END
 CCMPLX FUNCTION Q1DCM*16(DK,DR,DW,CK,RHO,OFFSET,SIGMA,N,Q1ABCF,C1RBCF,C1RBCF)

1 F(IPT) IT REAL*8(A - E,G,H,O,P,R - Y), COMPLEX*16(F,C,Z)
 C1ABCF(13),Q1RBCF(13)
 C1ABCF(13),FV(5),F1T(60),F2T(60),F3T(60),CESTT(60),CPSUM(60)
 C1ABCF(13),F1T(60),F2T(60),F3T(60),CESTT(60),CPSUM(60)
 C1ABCF(13),F1T(60),F2T(60),F3T(60),CESTT(60),CPSUM(60)

1 F(X) = X*(Q1DPHI(CK,DR,DW,RHO,OFFSET,SIGMA,N,C1ABCF,C1RBCF,X,ICT))
 - QALPHA*CIPT(0) WRITE(6,990) CK,DR,DW,RHO,OFFSET,SIGMA,N,ICT
 990 FCRMAT(0,DK,13X,DR,13X,CK,12X,OFFSET,9X,SIGMA,
 3 10X,N,3X),12,2X,13)
 4 10X,5,3X),12,2X,13)
 5 A = 1.0DC

1 ICT = IPT - 1
 GAMMA = 1.4C0
 LAMDA = CK/((GAMMA + 1.0D0) * CK)
 QALPHA = DCPLX(0.0D0,DLAMDA-DK)
 UACC = 9.0E-13
 ACC = 1.0D-5
 EFGURU = 1.0D-4.C*U

1 EFLAG = 1
 EFS = ACC
 GERROR = CCMPLX(0.0DC,0.0D0)
 LVLRR(LVL) = 1
 CPSUM(LVL) = 0.0
 ALPHA = A

1 AREA = B - A
 AREST = 0.0
 FV(1) = F(ALPHA)
 FV(3) = F(ALPHA + 0.5*DA)
 FV(5) = F(ALPHA + CA)
 KCUNT = 3

1 WT = DA/6.0
 QX = WT*(FV(1) + 4.0*FV(3) + FV(5))
 DX = 0.5*DA
 FV(2) = F(ALPHA + 0.5*DX)
 FV(4) = F(ALPHA + 1.5*DX)
 KCUNT = KCUNT + 2

1

LN0481C
 LN0482C
 LN0483C
 LN0484C
 LN0485C
 LN0486C
 LN0487C
 LN0488C
 LN0489C
 LN0490C
 LN0491C
 LN0492C
 LN0493C
 LN0494C
 LN0495C
 LN0496C
 LN0497C
 LN0498C
 LN0499C
 LN0500C
 LN0501C
 LN0502C
 LN0503C
 LN0504C
 LN0505C
 LN0506C
 LN0507C
 LN0508C
 LN0509C
 LN0510C
 LN0511C
 LN0512C
 LN0513C
 LN0514C
 LN0515C
 LN0516C
 LN0517C
 LN0518C
 LN0519C
 LN0520C
 LN0521C
 LN0522C
 LN0523C
 LN0524C
 LN0525C
 LN0526C
 LN0527C
 LN0528C


```

5  FV(5) = F3T(LVL)
   AREST = ARESTT(LVL)
   QEST = QESTT(LVL)
   EFS = EPST(LVL)
   GC TO 1 2
   IFLAG = 2 3
   GC TO 2 3
   IFLAG = 2
   GC TO 2
   END
   COMPLEX FUNCTION C1PHI*16 (DK,DR,CW,RHO,OFFSET,SIGMA,
1  N,Q1AECF,Q1RBCF,XSTN,IPT) COMPLEX*16(Q,Z)
   IMPLICIT REAL*8(A-H,O,P,R-Y), COMPLEX*16(Q,Z)
   DIMENSION Q1ABCF(13), Q1RBCF(13)
   IF (IPT.GT.C) WRITE(6,990) CK,DR,CW,RHO,OFFSET,SIGMA,XSTN,IPT
990  FCFMAT(0,10X,'Q1PHI ENTERED WITH:',/,RHO,10X,'OFFSET',7X,'SIGMA',
1  ,10X,'DK',11X,'DR',11X,'DW',11X,'RHO',11X,'I3')
2  ,8X,'XSTN',9X,'IPT',/,10X,'E12.5',11X,'I3')
   RZERC = 0.000
   ICT = IPT - 1
   C1PHI = Q1PREP(DK,CR,DW,RZERO,XSTN,IOT)
1  + Q1PAEP(DK,DR,CW,RZERO,OFFSET,XSTN,Q1RBCF,N,IGT)
2  + Q1PAEP(DK,DR,CW,DR,OFFSET,SIGMA,XSTN,IOT)
3  + Q1PAEP(DK,DR,DW,DR,OFFSET,SIGMA,XSTN,CLAEFC,N,IOT)
   IF (IPT.LE.0) RETURN
995  WRITE(6,995) C1PHI
   FCFMAT(0,10X,'Q1PHI = ',E14.7,11X,'E14.7)
   RETURN
   END
   COMPLEX FUNCTION Q1PRBP*16(DK,DR,DF,CW,RHO,XSTN,IPT)
   IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX*16(Q,Z)
   DIMENSION QINP(2)
   IF (IPT.GT.0) WRITE(6,990) CK,CR,CW,RHO,XSTN,IPT
990  FCFMAT(0,10X,'Q1PRBP ENTERED WITH:',/,RHO,10X,'XSTN',9X,'IPT',
1  ,10X,'DK',11X,'CR',11X,'DW',11X,'RHO',11X,'I3')
2  ,10X,'I5(E12.5',11X,'I3)
   IF (XSTN.LE.RHO-1.000) GO TO 20
   ICT = IPT - 1
   GAMMA = 1.40
   CM2 = (GAMMA + 1.000) * DW
   CLAMDA = CK/DM2
   PR = 1.0 + XSTN-RHO
   PIMAG = (CK+DLAMDA)*((XSTN-RHO)*(XSTN-RHO) - 1.000)
   Q1PRBP = - CCMPLEX(PR,PIMAG-CLAMCA*XSTN*PR)/CSRT(CM2)
   IF (IPT.LE.0) RETURN
   GCTC 60
20  Q1PREP = CCMPLEX(C,000,0.000)
   IF (IPT.LE.0) RETURN

```



```

60 WRITE (6,995) C1FFBP
995 FCRRMAT(0,10X,'Q1PRBP = ',E14.7,',',E14.7)
RETURN
ENC
COMPLEX FUNCTION Q1PAEP*16(DK,DR,DW,RHO,CFFSET,SIGMA,XSTN,IPT)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX*16 (Q,Z)
DIMENSION QINP(2)
IF(IPT.GT.0) WRITE(6,990) DK,DR,DW,RHO,OFFSET,SIGMA,XSTN,IPT
FORMAT(0,10X,'Q1PABP ENTERED WITH:',/
1,10X,'CK',11X,'DR',11X,'CW',11X,'RHC',10X,'CFFSET',7X,
2,SIGMA,8X,'XSTN',9X,'IPT',/,10X,7(E12.5,',',),I3)
XSTN = XSTN - OFFSET
IF(XASTN.LE.RHO-1.0D0) GOTO 20
ICT = IPT - 1
CCNST = CDEXP( DCMLPX(0.0D0, SIGMA))
GAMMA = 1.4D0
DM2 = (GAMMA + 1.0D0) * DW
DLAMDA = DK/DM2
PR = 1.0D0 + XASTN - RHO
FIMAG = (DK+DLAMDA)*((XASTN-RHC)*(XASTN-RHO) - 1.0D0)
Q1PAEP = DCMLPX(PR,PIMAG-DLAMDA*XASTN*PR)*(CCNST/DCRRT(EM2)
IF(IPT.LE.0) RETURN
GOTO 60
20 Q1PAEP = DCMLPX(0.0D0,0.0D0)
IF (IPT.LE.0) RETURN
60 WRITE (6,995) Q1FABP
995 FCRRMAT(0,10X,'Q1PABP = ',E14.7,',',E14.7)
RETURN
END
COMPLEX FUNCTION C1DPHI*16 (DK,DR,DW,RHO,CFFSET,SIGMA,
1 N,Q1ABCF,Q1RBCF,XSTN,IPT)
IMPLICIT REAL*8(A-H,O,P,R-Y), COMPLEX*16 (C,Z)
DIMENSION Q1ABCF(13),Q1RBCF(13)
IF (IPT.GT.0) WRITE(6,990) DK,DR,DW,RHO,CFFSET,SIGMA,XSTN,IPT
FCRRMAT(0,10X,'Q1DPHI ENTERED WITH:',/
1,10X,'CK',11X,'DR',11X,'CW',11X,'RHO',10X,'OFFSET',7X,'SIGMA',
2,8X,'XSTN',9X,'IPT',/,10X,7(E12.5,',',),I3)
RZERO = 0.0D0
ICT = IPT - 1
C1DPHI = Q1CRBP(DK,DR,DW,RZERC,XSTN,IOT)
1 + Q1DRIP(CK,DR,DW,RZERO,OFFSET,XSTN,Q1RBCF,N,IOT)
2 + Q1CABP(DK,DR,DW,DR,CFFSET,SIGMA,XSTN,IOT)
3 + Q1DAIP(DK,DR,DW,DR,OFFSET,SIGMA,XSTN,Q1ABCF,N,IOT)
IF (IPT.LE.0) RETURN
WRITE (6,995) Q1CPHI
995 FCRRMAT(0,10X,'C1DPHI = ',E14.7,',',E14.7)
RETURN
ENC

```



```

CCOMPLEX FUNCTION C1DREP*16(CK,DR,[W,RHO,XSTN,IPT)
IMPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX*16 (Q,Z)
DIMENSION C1NP(2)
IF (IPT.GT.0) WRITE(6,990) CK,DR,[W,RHO,XSTN,IPT
FCRMAT([C,10X,'Q1CRBP ENTERED WITH: ',/,
1,10X,[C,10X,'CR',11X,[W,RHO,XSTN,IPT,
2,10X,5(E12.5,' '),13)
/,XSTN,LE,RHO-1.000} GOTO 20
ICT = IPT - 1
GAMMA = 1.400
DM2 = (GAMMA + 1.000) * DW
CLAMDA = DK/DM2
CLM2 = (GAMMA + 1.000) * DW
PIMAG = (DK+DLAMDA)*(XSTN-RHO)
Q1CRBP = -DCMPLX(1.000,PIMAG-CLAMDA*XSTN)/DSQRT(DM2)
IF (IPT.LE.0) RETURN
GOTO 60
20 Q1CRBP = DCMPLX(0.000,0.000)
IF (IPT.LE.0) RETURN
60 WRITE(6,995) Q1DRBP
FCRMAT([C,10X,'Q1DRBP = ',E14.7,' ',E14.7)
RETURN
990 ENCL
CCOMPLEX FUNCTION C1DABP*16(DK,DR,[W,RHO,OFFSET,SIGMA,XSTN,IPT)
IMPLICIT REAL*8 (A-F,O,P,R-Y), COMPLEX*16 (Q,Z)
DIMENSION C1NP(2)
IF (IPT.GT.0) WRITE(6,990) DK,DR,[W,RHO,OFFSET,SIGMA,XSTN,IPT
FCRMAT([C,10X,'Q1CABP ENTERED WITH: ',/,
1,10X,[C,10X,'DR',11X,[W,RHO,XSTN,IPT,
2,10X,8),XSTN,9X,10X,7(E12.5,' '),13)
/,SIGMA,XSTN,OFFSET
XSTN = XSTN - CFFSET
IF (XSTN.LE.RHO-1.000) GOTO 20
ICT = IPT - 1
GCCNST = CDEXP( DCMPLX(0.000,SIGMA))
GAMMA = 1.400
DM2 = (GAMMA + 1.000) * DW
LLAMDA = DK/DM2
PIMAG = (DK+DLAMDA)*(XSTN-RHO)
Q1CABP = DCMPLX(1.000,PIMAG-CLAMDA*XSTN)*GCCNST/DSQRT(DM2)
IF (IPT.LE.0) RETURN
GOTO 60
20 Q1CABP = DCMPLX(0.000,0.000)
IF (IPT.LE.0) RETURN
60 WRITE(6,995) Q1DABP
FCRMAT([C,10X,'Q1CABP = ',E14.7,' ',E14.7)
RETURN
995 ENCL
CCOMPLEX FUNCTION C1PAIP*16([C,DR,[W,RHO,CFST,SGMA,XSTN,Q1CF,N,IPT)

```



```

IAPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX * 16 (C,Z)
DIMENSION Q1CF(13)
IF (IPT.GT.0) WRITE(6,990) CK,DR,CW,RHO,OFST,SGMA,XSTN,IPT
990 FCRMAT(0,10X,'Q1PAIP ENTERED WITH:',/,
1,1CX,'DK',11X,'DW',11X,'RHO',10X,'OFST',9X,'SGMA',5X
2,'XSTN',9X,'IPT',/,',,10X,7(E12.5,','),13)
XASTN = XSTN - OFST
IF(XASTN.LE.DR+RHO-1.000) GO TO 20
CONST = CDEXP( DCMPLX(0.000,SGMA))
GAMMA = 1.400
DM2 = (GAMMA+1.000)*DW
DLAMDA = DK/DM2
XX=XASTN-RHO
Q1 = Q1CF(1)
Q2 = Q1CF(2)
PR1 = XX+1.000-DR - XX/2.000)*XX - (CR-1.000)*(DR-1.000)/2.000
PR2 = (CR-1.000 - (XX*XX+(2.000-DR)*DR-1.000)*DLAMDA/2.000
FIMAG1 = XX*XX*((DR-1.000)/2.000-XX) - ((DR-1.000)*3)/6.000
PIMAG1=PIMAG1*DLAMDA
PIMAG2 = PIMAG2*CLAMDA
QP1 = DCMPLX(PR1,FIMAG1-DLAMDA*PR1*XASTN)
QP2 = DCMPLX(PR2,PIMAG2-DLAMDA*PR2*XASTN)
Q1PAIP = (Q1*QP1 + Q2*QP2)/DSQRT(CM2)
IF(IPT.LE.0) RETURN
GCTC 30
Q1PAIP = CCPLX(0.000,0.000)
IF(IPT.LE.0)RETURN
30 WRITE(6,995) Q1PAIP
995 FCRMAT(0,10X,'Q1PAIP = ',E14.7,',',E14.7)
RETURN
END
COMPLEX FUNCTION CIPRIP*16(CK,DR,CW,RHO,OFFSET,XSTN,C1CF,N,IPT)
IAPLICIT REAL*8 (A-H,C,P,R-Y), COMPLEX * 16 (Q,Z)
DIMENSION C1CF(13)
IF (IPT.GT.0) WRITE(6,990) DK,DR,DW,RHO,XSTN,IPT
990 FCRMAT(0,10X,'Q1PRIP ENTERED WITH:',/,
1,1CX,'DK',11X,'DR',11X,'DW',11X,'RHO',10X,
2,'XSTN',9X,'IPT',/,',,10X,5(E12.5,','),13)
IF(XSTN.LE.CR+RHO+CFSET-1.000) GO TO 20
GAMMA = 1.400
CM2 = (GAMMA+1.000)*DW
CLAMDA = DK/DM2
XX = XSTN - RHO
C2 = C1CF(2)
C1 = C1CF(1)
PF1 = XX+1.000-DR
PR2 = (CR-1.000 - XX/2.000)*XX - (DR-1.000)*(DR-1.000)/2.000

```



```

FIMAG1 = (XX*XX+(2.000-DR)*DR-1.000)*DLAMDA/2.000
PIMAG2 = XX*XX*((DR-1.000)/2.000-XX)-((DR-1.000)**3)/6.000
PIMAG1=PIMAG1*DLAMCA
PIMAG2 = PIMAG2 * CLAMDA
CP1 = DCMPLX(PR1,PIMAG1-DLAMDA*PR1*XSTN)
CP2 = DCMPLX(PR2,PIMAG2-DLAMDA*PR2*XSTN)
Q1PRIP = -(Q1*QPI+C2*CP2)/DSQRT(EM2)
IF(IPT.LE.0) RETURN
GCTO 30
C1FRIP = DCMPLX(0.000,0.000)
IF (IPT.LE.0) RETURN
WRITE (6,995) Q1PRIP
FCRMTAT('0',10X,'Q1PRIP = ',E14.7,' ',E14.7)
RETURN
END
CCOMPLEX FUNCTION Q1DAIP*16(DK,DR,CR,RHO,OFST,SGMA,XSTN,CICF,N,IPT)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX * 16 (C,Z)
DIMENSION Q1CF(13)
IF (IPT.GT.C) WRITE(6,990) DK,DR,CR,RHO,CFST,SGMA,XSTN,IPT
FCRMTAT('0',10X,'Q1CAIF ENTERED WITH:',/,
,10X,'DR',11X,'DW',11X,'RHO',10X,'OFST',9X,'SGMA',5X
,XSTN,9X,'IPT',/,
,XSTN,XSTN-OFST
XSTN=XSTN-OFST
IF(XASTN.LE.DR+RHC-1.000) GC TO 20
GCCNST = CDEXP( DCMPLX(0.000,SGMA))
GAMMA = 1.400
CLAMDA = (GAMMA+1.000)*CW
CLAMDA = DK/DM2
XX = XASTN - RHO
Q1 = Q1CF(2)
Q1CF(1)
PR1 = 1.000
PR2 = DR-1.000-XX
PIMAG1 = DLAMDA*XX
PIMAG2 = DLAMDA*(DR-1.000-XX)*XX*XX
CP1 = DCMPLX(PR1,PIMAG1-DLAMDA*PR1*XASTN)
CP2 = DCMPLX(PR2,PIMAG2-DLAMDA*PR2*XASTN)
Q1CAIP = (Q1*QPI + Q2*CP2)/DSQRT(EM2)
IF(IPT.LE.0) RETURN
GCTO 30
Q1DAIP = CCMPLX(0.000,0.000)
IF (IPT.LE.0) RETURN
WRITE (6,995) Q1DAIP
FCRMTAT('0',10X,'Q1DAIP = ',E14.7,' ',E14.7)
RETURN
END
CCOMPLEX FUNCTION G1DRIP*16(DK,DR,CR,CW,RHO,OFFSET,XSTN,CICF,N,IPT)
IMPLICIT REAL*8 (A-H,O,P,R-Y), COMPLEX * 16 (Q,Z)

```



```

DIMENSION QICF(13)
IF (IPT.GT.0) WRITE(6,990) DK,DF,CW,RHO,XSTN,IPT
FORMAT(0,10X,'CLDRIP ENTERED WITH:',/,RFO,10X,
1 10X,'CK,11X,'DR,11X,'CW,11X,'RFO,10X,
2 'XSTN,19X,'IPT',10X,'5(E12.5),13)
IF(XSTN.LE.(R+RHO+OFFSET-1.000) (010 20
GAMMA = 1.400
CM2 = (GAMMA+1.000)*DW
CLAMDA = DK/CM2
Q1 = QICF(1)
Q2 = QICF(2)
XX = XSTN - RHO
PR1 = 1.000
PR2 = DR-1.000-XX)*XX*XX
PIMAG1 = CLAMDA*XX
PIMAG2 = CLAMDA*PR1*XSTN)
QF1 = CCMPLEX(FR1,PIMAG1-CLAMDA*PR1*XSTN)
QF2 = CCMPLEX(FR2,PIMAG2-CLAMDA*PR2*XSTN)
QICRIP = -(Q1*QF1+Q2*QF2)/CSQRT(DM2)
IF (IPT.LE.0) RETURN
GCTC 30
CLDRIP = CCMPLEX(C.000,0.000)
IF (IPT.LE.0) RETURN
30 WRITE(6,995) QICRIP
955 FORMAT(0,10X,'QICRIP = ',E14.7,1,1,E14.7)
RETURN
END

```

```

LIAC08170C
LIIN08180
LIIN08190
LIIN08200
LIIN08210
LIIN08220C
LIIN08230
LIIN08240
LIIN08250
LIIN08260
LIIN08270
LIIN08280C
LIIN08290
LIIN08300
LIIN08310
LIIN08320
LIIN08330C
LIIN08340
LIIN08350C
LIIN08360
LIIN08370
LIIN08380
LIIN08390
LIIN08400
LIIN08410
LIIN08420C
LIIN08430

```


LIST OF REFERENCES

1. Elder, P. R., A Theoretical Analysis of Unsteady Transonic Cascade Flow, Thesis, Naval Postgraduate School, Monterey, California, 1972.
2. Schlein, P. B., A Study of Unsteady Transonic Interference Effects, Thesis, Naval Postgraduate School, Monterey, California, 1975.
3. Landahl, M., Unsteady Transonic Flow, Pergamon Press, 1961.
4. Gorelov, D. N., "Oscillations of a Plate Cascade in a Transonic Gas Flow," Mekhanika Zhidkosti i Gaza, v. 1, no. 1, pp. 69-74, 1966.
5. Garrick, I. E. and Rubinow, S. J., Flutter and Oscillating Air-Force Calculations for an Airfoil in Two-Dimensional Supersonic Flow, NACA Report 846, 1946.
6. Stevens, W. P.G. J. Meyers, and L. L. Constantine, "Structured Design," IBM Systems Journal, No. 2, pp. 115-139, 1974.
7. Shampine, L. F., and R. C. Allen, Numerical Computing: An Introduction, W. B. Saunders Company, 1973.
8. Ashley, H. and Landahl, M., Aerodynamics of Wings and Bodies, Addison-Wesley Publishing Company, Inc., 1965.
9. Miles, J. W., "The Compressible Flow Past an Oscillating Airfoil in a Wind Tunnel," Journal of Aeronautical Sciences, v. 23, no. 7, pp. 671-678, 1956.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Documentation Center Cameron Station Alexandria, Virginia 22314	2
2. Library, Code 0142. Naval Postgraduate School Monterey, California 93940	2
3. Professor M.F. Platzler, Code 57P1 Department of Aeronautics Naval Postgraduate School Monterey, California 93940	10
4. Lt. Peter C. Olsen USCG 16207 Pointer Ridge Drive Bowie, Md. 20716	4
5. Assoc. Professor F.R. Richards, Code 55rh Department of Operations Research Naval Postgraduate School Monterey, Ca. 93940	1
6. Mr. Robert C. Olsen Quality Engineering, WSOB Pratt and Whitney Aircraft East Hartford, Conn. 08106	1
7. Professor D.J. Collins, Code 67Co Department of Aeronautics Naval Postgraduate School Monterey, Ca. 93940	1

Thesis

0484

c.1

Olsen

278764

Theoretical analysis of
transonic flow past
unstaggered oscillating
cascades.

Thesis

0484

c.1

Olsen

278764

Theoretical analysis
of transonic flow past
unstaggered oscillating
cascades.

thes0484

Theoretical analysis of transonic flow p



3 2768 001 97502 2

DUDLEY KNOX LIBRARY